

# DAVIDSON LABORATORY

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November 1982

TESTS OF TOWED ARRAYS OF
AIR CUSHION AMPHIBIOUS VEHICLES
IN CALM WATER AND WAVES

by G. Fridsma and W.E. Klosinski

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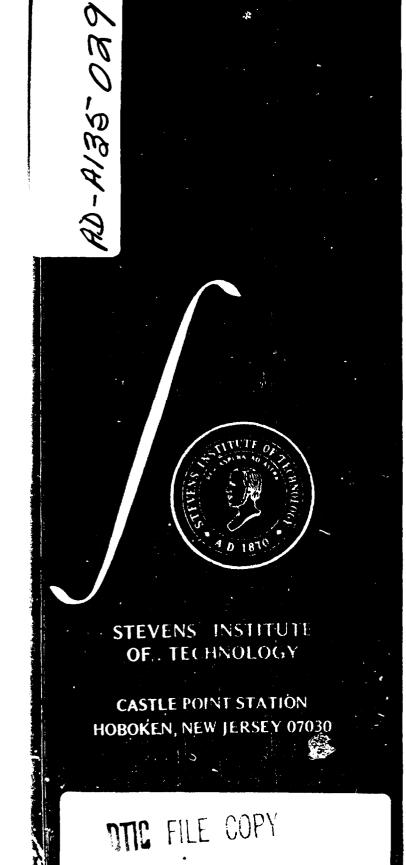
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# STEVENS INSTITUTE OF TECHNOLOGY DAVIDSON LABORATORY

Castle Point Station, Hoboken, New Jersey 07030

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G. Fridsma and W.E. Klosinski

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#### INTRODUCTION

A series of investigations into the hydrodynamic and vehicle mobility characteristics of tracked amphibious vehicles is being carried out by the Davidson Laboratory in support of the Marine Corps Surface Mobility Exploratory Development Plan. These investigations have been initiated under the direction of the David W. Taylor Naval Ship Research and Development Center (NSRDC), Code 112 which manages the Mobility Program. A bibliography of the results achieved in previous investigations is reported herein.

The present tests undertake to provide basic technology contributing to the development and implementation of improvements in the surface mobility of amphibious vehicles by supporting them on an air cushion and coupling them together in a towed array. Measurements of the towing force (drag) and seakeeping characteristics in Sea State 2 were the primary objectives.

Supporting an amphibious tracked vehicle on an air cushion has some advantages over the conventional vehicle because the bow burying and deck wetness problems are eliminated. The total effective drag of the air cushion vehicle (ACV), which may be expected to be of the same order as that of the conventional displacement hull at speeds up to 15 mph. is significantly reduced at higher speeds. Consequently the towing force, which does not include fan drag, is expected to be lower over the speed range up to 45 mph. The propulsion of an ACV amphibian presents serious problems however, since air propulsion is out of the question and water propulsion requires retractable drive-shafts passing through the support bubble. In order to realize the potential benefits of ACV support while avoiding the propulsion problem, Code 112 suggested that the ACV amphibian should be towed rather than be self-propelled. This "tug and barge" concept led to the concept of a vehicle train which would reduce the unit vehicle drag. Candidates considered for the role of towing the train of ACV's included a helicopter and an air-cushion landing craft (LCAC).

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in addition to speed and type of tow, other parameters investigated included number of vehicles in the train (up to four), inter-vehicle spacing, and track position, whether retracted or extended.

Tests were carried out in the Tank 3 facility of the Davidson Laboratory during the period 9 to 22 September 1982. Mr. Walter Zeitfuss, Jr. (NSRDC, Code 112) and Mr. Nic Economou (Bell Aerospace, Textron) were present for part of the tests to monitor the behavior of the ACV's and to offer technical assistance.

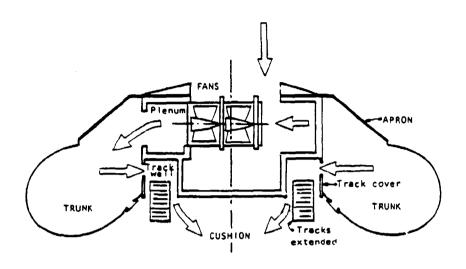
#### MODELS

Four identical 1/8 scale test models of the ACV were fabricated at the Davidson Laboratory according to drawings supplied by Bell Aerospace (Buffalo) and NSRDC. The configuration consisted of a hull very similar to the small amphibian "FLASH" (Reference 2) supplemented by an inflatable trunk to retain the air cushion. Views of one of the complete ACV models are included on Figures 1 and 2.

Lucite was used in the construction of the hull, neopeene impregnated cloth was used for the trunk, and aluminum was used for the trunk support (apron) and other fastenings. The photograph on Figure 3 shows the model's constituent parts.

In order to make the trunk, a wooden mold was constructed which included the shape of the trunk itself and those parts of the apron and hull to which the trunk would be attached. The 0.008 inch thick neoprene cloth was applied on the mold, cut and seamed, and then fitted to the attachment points. The mold as constructed to the drawings supplied by Bell, however, failed to produce a smooth rounded trunk that was tangent to the ground plane. Modifications to the mold were necessary to achieve this smoothness, particularly in the four corners where the various segments of cloth joined. After some trial and error, a good fit was obtained and four trunks were constructed. Excess material was provided at the attachment points for final fitting to the model with the trunk inflated. The resulting trunk achieved a good tangent plane when placed on a carpeted surface table. Final assembly included the gluing and sewing of surgical tape over the seams, inside and out, for additional reinforcement of these joints.

A lucite fan-housing box was built inside the model and attached to the starboard side of each model, just above the tracks. Holes for two fans were cut in this nousing which supported two sets of stacked fans, for a total of four Aximax 3 fans in each model. Air through these holes supplied the trunk, whose upper half was attached to the hull at the apron and whose lower half was attached to the bottom of the track covers and the hull at the bow and stern. The following sketch shows the air supply to the trunk and cushion.



Provision for adjusting the trunk pressure was made by a hole, cut in the apron, on the stern centerline to vent air from the trunk to atmosphere. To supply air from the trunk to the cushion, the original design called for holes to be cut in the trunk fabric, as indicated in the sketch. Because of the possibility of water getting into the trunk, Davidson Laboratory recommended that the cushion feed holes be sealed and holes in the track covers be provided. This modification to the design was discussed with Bell Aerospace and thought to be an improvement in the design. As a result eighteen 6 inch diameter holes (full scale) were drilled to provide the inlet area specified by Bell for air from the trunk to the cushion, 6 in each of the port and starboard track covers and 6 at the bow. Here and hereafter all quantities are given in full scale terms. The holes were positioned longitudinally in the track covers at the approximate locations specified in the Bell drawings. Some minor adjustment was necessary in order for the air to be supplied between the road wheels, otherwise the airflow would be throttled by the wheels when the tracks were retracted.

To duct air through the bow structure, from the trunk to the cushion, an enclosed compartment was built inside the lower hull which straddled the lower trunk attachment point on the bow. The upper half of this compartment had a 280 square inch slotted hole milled in it which opened into the trunk. The lower half had six 6 inch diameter holes drilled in it which opened into the cushion.

During the fan calibration tests, it was found that the design pressure drop between the trunk and cushion could not be achieved with the specified holes. Consequently the holes in the track covers were enlarged to 8 inch diameter, which provided the proper pressure drop. The total inlet area to the cushion became 5.36 square feet, full size.

The track-suspension system, road wheels and tracks, were attached to a horizontal plate which could be mounted to the hull to simulate either the fully extended or retracted track positions. Photographs showing the cushion air-supply inlet area and the suspension system are shown on Figure 4.

Two pressure taps were mounted in the model. The trunk pressure tap was located on the port side, 15 inches forward of the transom and 39 inches above the hull bottom. The cushion pressure tap was located in the hull bottom on the craft centerline, 35 inches forward of the transom. These can be seen in the top photo of Figure 4.

The models were ballasted to a 30,000 lb displacement, with a VCG 28 inches above the hull bottom, and an LCG 110 inches aft of the bow hard structure. Other ACV particulars can be found in the table following the text of this report.

During on-cushion check out tests on a surface table, a vibration was observed in the forward trunk region. A narrow aluminum "finger" curved in the shape of the trunk was fastened to the apron at the bow and effectively suppressed the oscillation (see Figures 1 and 2). It was demonstrated by Mr. Economou that the same effect could be achieved by adding a small weight to the trunk at the bow.

#### Fan Calibration

An overall calibration of the fan system was requested by Bell Aerospace. The fans were calibrated, while they were mounted in a model, by the use of a specially constructed calibration box (see Figure 6). This air tight box was fabricated from 1/2 inch plywood and consisted of a large upper compartment into which the test model was placed and a smaller lower compartment, which served as an extension of the cushion plenum. The lower plenum was equipped with a pressure tap and various sized orifices through which the air discharged into the atmosphere. To provide an air-tight seal between the model and upper compartment, neoprene impregnated material was fastened between the metal apron of the model and the external periphery of the upper compartment. This ensured that all of the air flow exited either through the holes in the lower compartment, or through the trunk pressure adjustment orifice located in the aft end of the model apron.

The pressure-flow relationship for the trunk and cushion could be controlled by either changing the hole diameter in the vertical track covers or by varying the area of the trunk vent in the stern apron

After spending some time calibrating the system and experimenting with the variables, a combination was obtained which produced a pressure—flow curve very similar to the prototype requirement (see Figure 7). The trunk to cushion area was 5.37 square feet and the trunk vent area was 1.79 square feet. The experimental design point (full size) was 119 psf for the trunk pressure and 72 psf for the cushion at a flow rate of 610 cfs.

#### MODEL TEST PROCEDURES

A ground board was constructed inside the dock end of Tank 3, just above the still water surface, for the purpose of stowing the models when off cushion prior to and after the end of each test run. This was necessary because a back flow of water through the cushion air-supply holes when the fans were off could cause the trunks to fill with water and the model to sink. The test procedure was as follows. With the models resting on the ground board and the fans off, zeroes were taken. The fans were then turned on, and the models were slowly towed off the board and into the water to the starting position of the run. At the end of the

run, the models were towed back to the dock and up onto the ground board, where the fans were shut off.

The ACV models were towed by lines, simulating a tow by either a helicopter or an LCAC, singly or in a train of up to four vehicles. helicopter tow consisted of a single line 100 feet long attached on the lead craft centerline at the bow and angled upwards at 10 degrees. LCAC tow consisted of a V-shaped bridle attached 18 1/2 feet apart at the LCAC and on the bow centerline of the lead ACV. This tow line was 30 feet long with a 7 degree upward slope. The tow lines between the ACV's were all V-shaped bridles attached on the bow centerline and spread 8 feet across at the stern of the ahead ACV. The lengths of the towing bridles were adjusted to achieve three spacings between the ACV's resulting in hard hull structure spacings of 42.7 feet, 22.7 feet and 13.3 feet and trunk to trunk spacings minimum distances between ACV's) of 30.7 feet. 10.7 feet and 1.3 feet respectively. Nylon cord was used for all model tow lines (rather than stainless steel wire) in order to simulate a degree of stiffness somewhat representative of the prototype lines. were fitted at the ends with heavy-duty swivels and snap-hooks for quick attachment to the eye bolts in the models.

#### APPARATUS AND INSTRUMENTATION

The train of ACV LVT's was to be towed by either a helicopter or an LCAC. The towing vehicle was simulated by a spreader bar attached to a drag balance for measuring the horizontal component of the tow line tension. The spreader bar was equipped with three eye bolts located symmetrically under the balance, one on the centerline for the helicopter tow, and two outboard for the LCAC tow.

Since the models were towed by flexible lines, they had all six degrees of freedom. No yaw restraint was employed to allow for observations of the tracking stability.

The trunk and cushion pressures in each model were measured in the calm water tests as well as the drag or towing force. In Sea State 2 additional measurements were taken of the vertical accelerations in each ACV at the driver's station, and the vertical and horizontal accelerations in the troop compartment. The vertical units were located, respectively, 4.7 and 13.8 feet aft of the bow hard structure. A wave strut was used to

monitor the waves and to record encounters.

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The signals from the transducers were relayed by overhead cable to the data station on shore, where they were filtered (40 Hz low pass) and processed by an on-line PDP-8e computer, which includes an analog to digital converter. The rough water data, which were scanned at 250 Hz, were stored on the computer's disks. For the four-unit train, twenty-two channels of data were measured and recorded. Test run data were monitored on a direct writing oscillograph.

### Photography

Video tape recordings were made of ach run by a television camera mounted ahead and to port of the lead model. Selected above—water color still photographs were taken of the models in calm water and in waves, see Figure 5.

#### Wavemaker

The newly installed Davidson Laboratory Tank 3 wavemaker was used for these tests. This is an articulated double flap wet-back wavemaker, consisting of upper and lower flaps each powered by a hydraulic cylinder. A PDP 11/23 computer generates the signals for controlling the movement of the hydraulic actuator-flap system and, therefore, the size and shape of the waves. For the present tests, a wave train, having a variance density approximating the Pierson-Moskowitz spectrum with a 2.2 foot significant wave height, was used corresponding to Sea State 2 (see Figure 17).

#### DATA REDUCTION

Calibrations of the instrumentation were made by applying known loads to the force balance, gravity multiples to the accelerometers, and known pressures to the pressure transducers. During calibration, the outputs from the transducers were relayed to the PDP-8e computer. All calibrations were linear, and straight lines were fitted to three data by the least squares technique.

Test results were determined from the differences between transducer outputs in the running and static, off-cushion conditions. Velocities were computed from the time taken to travel through the data trap, which

was 50 feet for the calm water tests and 150 feet for the wave tests.

Processing of the calm water data produced mean values for the drag, and for the trunk and cushion pressures in each ACV. For the wave tests, a peak-trough analysis was performed on the drag, the trunk and cushion pressures, the troop and driver vertical accelerations, and the horizontal acceleration in each ACV. A peak-trough analysis of each signal resulted in the mean and rms, the number of oscillations, the average of the peaks and troughs, the average of the 1/3 highest and the 1/10 highest peaks and troughs, and the extreme values of the peaks and troughs. Buffers were used to suppress small oscillations associated with noise rather than the substantive time histories.

Repeat runs were made in different portions of the irregular wave train, at speeds above 15 mph, to get adequate samples of data for statistical analysis.

In addition to the above data processing, air flow and fan drag were computed for all tests. The following equations were used:

Cushion Flow = 95 \* SQRT (PT - PC)

Fan Drag = (PT x Flow)/V

where: PT = Trunk Pressure, psf
PC = Cushion Pressure, psf
V = Forward Speed, fps

Mean values of pressure were used for these computations in the wave tests.

#### RESULTS

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The results of the tests in calm water and waves are presented in Tables 1 to 9. Each table is labeled as to the number of units in the train, the type of tow, the spacing between vehicles, and the position of the tracks. The calm water data (Tables 1-6) have been sorted by values of increasing speed for each of the six configurations tested. The model quantities have been expanded to full size by the following ratios

Ship Drag = 526 \* Model Drag

Ship Pressure = 8 \* Model Pressure

Ship Flow = 181 \* Model Flow

Ship Fan Drag = 512 \* Model Fan Drag

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The fan drag is included because it is useful in determining the efficiency of the vehicle in terms of the lift/drag ratio. The fan drag is simply a conversion of the fan horsepower into an "equivalent" drag. The decrease in hydro-drag must be offset by the fan drag in order to account for the energy being expended to sustain the air cushion beneath the vehicle. To obtain the true lift/drag ratio the "total" drag can be divided into the weight. Thus in Table 1 for speeds of 10, 20 and 30 mph, the lift/drag ratios are respectively 2.9, 4.9 and 5.7.

Spacing in this report refers to the inter-vehicle spacing between the hard structure, i.e. between the bow and stern of the hull in the absence of the apron and trunk.

The data for the rough water tests are included in Tables 7 to 9, each table applying to a particular length for the ACV train. Each page presents the full scale values for a given set of test conditions such as speed, weight, LCG, and sea state. The mean drag or horizontal component of the towing force and the number of wave encounters are displayed at the top of the page along with a statistical analysis of the drag variations. Normally drag statistics are not presented because of the frequency response of the drag balance. For the tests reported herein, the elastic nylon cord tow line determines the frequency response. The model nylon tow line had a stiffness corresponding to 1,600 lb/in full size.

The rest of the page in Tables 7 through 9 presents, for each vehicle in the train, the statistics of the driver and troop acceleration, the horizontal acceleration, and the cushion and trunk pressures. The statistics include the mean and RMS values and the average, the average of the 1/3 highest, the average of the 1/10 highest, and the extreme values of the peaks and troughs. Blanks in the table of statistics generally indicate that the sample size was too small (a minimum of 5 oscillations must be observed to record a statistic).

The calm water performance of the ACV train is plotted on Figures 8 to 16. The performance in Sea State 2 is presented on Figures 18 to 25.

A video tape recording of all runs has been sent to NSRDC. Code 112, together with still photographs of selected runs. A scenario for the video tape is contained in the Appendix.

#### DISCUSSION

The pressure-flow requirements specified by Bell for the ACV are shown on Figure 7 along with the actual model fan calibrations. The calibrations match the specification at the design point, and the slopes of the pressure-flow curves for the trunk and cushion are in reasonable agreement with those specified. Under operating conditions, at speeds above 20 mph, the trunk and cushion pressures were 119 and 78 psf respectively at a cushion flow of 608 cfs. These are the precise design requirements for the ACV. They were achieved, however, with a 52 percent increase in the design cushion inlet area of 3.53 square feet. The discharge coefficient for the model was determined from these numbers and was equal to 0.61, the value expected from a ninety degree sharp-edged orifice. Pressure-flow measurements at the hover condition produced consistent readings of 110 and 65 psf for the trunk and cushion pressures respectively and 637 cfs for the cushion air flow.

Before discussing the specific performance characteristics, some comments about the general behavior of the ACV train are offered. These comments relate to the two-unit train in calm water over a range of speeds, and are based on observations made during the test trials. In general they also apply to three and four unit trains.

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Speed is the predominate parameter affecting the ACV's behavior in At 5 mph the ACV's ride at a level trim much like the hover condition. Spray is thrown forward as well as out from the model all around the periphery of the trunk. In general tracking (the ability of the trailing vehicles to align themselves behind the lead vehicle) was poor at this speed. Tracking, however, improves with speed and decreased spacing. At 7.5 mph an unusual "tuck under" oscillation occurs at the forward end of the trunk on the lead ACV. It appears as though suction forces due to the flow under the trunk create a bow down moment forcing the trunk into the water. The trunk is then seen to suddenly "pop up", possibly when the suction is overcome by the increased buoyancy. cycle is repeated as the models proceed down the tank. The following units, riding in the wake of the lead ACV, do not exhibit this phenomenon. Spray continues to be thrown out around the trunk periphery but diminishes with Increasing speed. Tracking is noticeably improved. At 10 and 11 mph, the ACV is operating just below or at the hump speed. A lot of water is seen to pile up against the front of the trunk. The "tuck under" phenomenon has disappeared, but the second unit of the train is still prone to wander a bit. As the speed is increased to 12.5 mph, the wave generated at the bow gets smaller and the second ACV of the train rides at a high trim angle. At 15 mph a small bow wave is still present and tracking is improved. Between 20 and 45 mph, the bow wave disappears, spray is generally deflected aft, and the models run cleanly. The higher the speed of the ACV, the better its behavior in terms of spray and tracking. In general the helicopter towed train tracked less well than the LCAC towed train, probably because of the single line tow as compared to a bridle tow.

in addition to speed, the spacing between vehicles has a significant effect on performance. Trains with the shortest spacing (13.3 ft) tracked better than trains with the longer spacings (22.7 and 43.8 ft). There was a considerable amount of spray generated between vehicles, however, at the 13.3 ft spacing. This can be attributed to the fact that with the trunks close together, the air flowing under the trunk trailing edge of the lead vehicle interacts with the spray generated at the bow of the following vehicle. Inter-vehicle spacing also has a dramatic effect on the drag characteristics particularly at the hump speed. Closer spacing reduces the hump drag.

While the effect of raising the track-suspension system level with the hull bottom did not effect the overall performance of the ACV's, it appeared that tracking deteriorated.

These qualitative comments are the result of observations or impressions obtained during the period of tank testing. The quantitive results are presented on Figures 8 to 25.

The calm water behavior of drag and pressure as a function of speed is shown in absolute terms for each of the six configurations in Figures 8 through 13. The drag curve has a destinctive characteristic that is very typical of ACV type craft (Reference 3). Starting from zero speed, the drag rises quickly to a rather sharply defined peak at the hump speed of 11 to 12 mph.

Above hump speed the drag falls dramatically and at 20 mph is approximately one half its maximum value. As speed increases beyond 20 mph, the drag rises moderately until the maximum test speed of 45 mph is reached. There does not appear to be an appreciable change in the hump speed with changing configuration. Also typical of ACV craft is the way the cushion pressure varies with speed. Starting from the hover condition the cushion pressure decreases slowly at first, then drops suddenly until a minimum is reached at the hump speed. This is followed by an abrupt recovery, however, when the cushion pressure rises with speed up to 20 mph. At the higher speeds the cushion pressure stays more or less constant. This characteristic applies to the single ACV and to the lead vehicle for the train configurations. Because of the inter-dependence between the trunk and cushion pressure for this particular ACV design, the trunk pressure's behavior parallels that of the cushion.

The pressure characteristics for the lead ACV are not necessarily those of the other units in the train. From Figures 8 to 13, it is clear that there is less fluctuation of the cushion and the trunk pressure with speed for the second and third units in the train than there is for the lead vehicle. Riding in the wake of an ACV therefore tends to smooth out the mean trunk and cushion pressures with speed.

Starting with Figure 14 some drag comparisons are made between the various configurations. The specific resistance or drag per ton of displacement is a useful quantity to plot versus speed. The drag is shown

to be independent of the type of tow for the 2 unit train (Figure 14). The drag reduction usually associated with coupled vehicles (on a specific basis) is not realized with the ACV trains. While some reduction is shown up to speeds of 25 mph, it does not compare with the order of magnitude experienced for the coupled LVT7 (Reference 1). The reason for this is that the nominal spacing of the ACV units of 22.7 feet is on the order of 1 cushion length. This would be equivalent to spacing the LVT7's 1 boat length apart. It is not until the ACV's are brought closer together that any real drag reduction is realized. Figure 18 shows the 4 unit train in Sea State 2 for the nominal and shortest spacing. Here the effect of the closer spacing is to reduce the hump drag significantly (about 37 percent). Lengthening the inter-vehicle tow line for this two-unit train, to make the spacing about 2 cushion lengths, increases the hump drag and in general degrades the performance (Figure 15).

The effect of retracting the tracks level with the hull bottom is presented on Figure 15. There is little change in drag until above hump speed, and then there is a slight improvement over the limited speed range of 18 to 35 mph after which the drag with tracks up is greater than that with tracks down. Because of the poorer course keeping of the two unit train with the tracks retracted and the lack of drag reduction, together with the added complexity and weight associated with track retraction, the remaining configurations were tested with the tracks extended.

An analysis of the fan drag for all calm water configurations is presented on Figure 16. The height of the rectangles in the upper plot is an indication of the amount of variation between test conditions. The assumed linear decrease of fan horsepower with speed shown in the lower plot is consistent with the curve in the upper plot. This curve fits the data remarkably well, which confirms the assumed linear relation. Thus, as speed is increased, less horsepower is required to maintain the ACV cushion. This is consistent with the reduction in air flow with speed due to less leakage from the cushion.

in rough water, 3 configurations were tested, three and four unit trains with a spacing of 22.7 ft, and a four unit train with a 13.3 ft spacing. These results are presented in Figures 18 to 25.

figures 18 and 19 present the drag results in Sea State 2. For the three-unit train, a drag comparison can be made between operations in calm water and Sea State 2. There is only a minimal increase in drag (8.5 percent at hump) at the low speed (Figure 18), from 20 to 35 mph, waves create a 20 to 35 percent increase in ACV resistance over that in calm water. It bears repeating that the drag reduction per ton of weight expected from running trains rather than single vehicles is not realized at the nominal spacings of 22.7 feet. It is when the vehicles are at their closest spacing that the specific drag is reduced significantly.

To design a tow line for the ACV train, the dynamic drag must be taken into account. The significant drag variations are plotted on Figure 19 where the maximum values are those of interest. It would appear that for three and four vehicle trains, a tow line able to take dynamic loads of 40,000 lb would be in order.

(A)の10間におれるのの100mmであるというでは、10mmになるとの10mmでは、10mmには10mmであるのでは10mmである。

FOR STANFAR COLOR

The rms and significant cushion and trunk pressure variations are included in Figures 20 and 21 respectively. The pressure fluctuations build up with increasing speed. The lead ACV experiences the largest pressure fluctuations. The fluctuations of the other three ACV's are almost identical. For speeds above 25 mph it is possible for the fluctuating cushion pressure to be zero or reach negative values. The significant maximum values over the same speed range are about double their mean values for vehicles 2, 3 and 4 in Sea State 2 and about triple their mean values for vehicle 1.

The acceleration data is presented on Figures 22 to 25 with trends similar to those for the pressures. The worst ride as measured by acceleration occurs near the bow where significant accelerations of 3 g's at 45 mph are experienced in the first and second units. These are gradually reduced to 1.5 g's as one proceeds along the train to the last unit. Accelerations in the lead ACV are comparable to those measured on the FSACV (Reference 3).

Figure 24 is presented to show that the accelerations experienced in a Sea State 2 are independent of spacing and the number of vehicles in the train. That is to say, the seakeeping results for the 4 unit train with shorter spacing are very similar to the results for the three and four vehicle train at the longer spacing, as typified by the behavior of the third unit in either train. An examination of the tabulated data

indicates that the drag, pressure and horizontal acceleration variations are also independent of vehicle spacing and number.

The horizontal accelerations depicted in Figure 25 are typical for all three configurations in Sea State 2 and are practically identical in all four units of the train. The significant values vary from  $\pm 0.2$  to  $\pm 0.6$  g's over the speed range from 5 to 45 mph. With positive accelerations being in the direction of motion, there does not appear to be a bias or preferred direction, fore and aft.

#### CONCLUDING REMARKS

Towing trains of amphibious tracked vehicles, supported by an air cushion, is a hydrodynamically viable alternative to the separately self-propelled amphibians currently employed for assault operations. The tow-line force (drag) is independent of how the trains are towed and is most affected by speed. Maximum drag occurs at the hump speeds between 11 and 12 mph, and the hump speed is not altered significantly with changes in either vehicle spacing or number. Close inter-vehicle spacing of the ACV's, together with increasing the number of vehicles in the train improves the specific resistance.

Seakeeping behavior is independent of the spacing and number of units in the train. The lead ACV experiences the worst ride with significant accelerations exceeding 2 and 3 g's over the speed range from 20 to 45 mph. Other units operating in the wake of the lead ACV have similar pressure variations, but progressively smaller accelerations toward the rear of the train. Excursions from the mean drag are also insensitive to spacing and number of units in the train.

Fan horsepower, required to maintain the cushion, decreases linearly with speed. When converted to a "equivalent drag" and added to the hydrodynamic drag, the total drag can be divided into the weight to obtain a lift/drag ratio. For the 4 unit train in Sea State 2 at the 13.3 ft spacing, overall lift/drag ratios of 3.9, 5.3 and 5.6 are obtained at 12.5 mph (hump speed). 20 mph and 30 mph respectively: this performance is comparable with that of a planing LVT.

#### TR-2299

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TR-2299
TABLE OF PARTICULARS

	Prototype	Mode 1
Displacement, 1b.	30,000	57.1
Length of ACV, in.		
Hard Structure	204	25.5
Overall Including Trunk	349	43.6
Beam of ACV, in.		
Hard Structure	106	13.25
Overall including Trunk	242	30.25
Depth of ACV to Deck, in.		
Hard Structure	58.5	7.31
Overall Including Trunk	81.5	10.19
Center of Gravity, in.		
Aft of Bow Hard Structure	110	13.75
Above Hull Bottom	28	3.50
Hull Clearance Above Tangent Plane	23	2.88
Design Pressures, psf		
Trunk	117	14.6
Cushion	79	9.9

TABLE 1

CALM WATER SINGLE ACV, HELICOPTER TOW TRACKS DOWN

	MAH	INRAG	L.B	10260.	7140.	4510.	4470.	4400.	3640.	2670.	2190.	1830.	1450.	1340.	1250.	1250.
-		FLOW	CFS	671.	685.	639,	694.	.669	655.	645.	657.	656.	609	636	598.	676.
	TRUNK	PRESS	PSF	112.	115.	104.	104.	115.	122.	122.	122.	123.	122.	123.	123.	122.
	CUSH	PRESS	PSF	62.	63.	58.	51.	61.	75.	76.	74.	75.	81.	78.	83.	71.
•		DRAG		_			_	_	_	_	_		3320.	_	_	_
	٠	SPEED	MFH	5.00	7.50	10.00	11.00	12.51	15.00	20.01	25.02	29.71	35.04	40.04	•	45.10
		RUN		Ø	2 <b>1</b>	M	14	13	4	เว	9	7	8	15	10	11

TABLE 2

CALM WATER
TWO UNIT ACV TRAIN, HELICOPTER TOW
22.7 FT SPACING, TRACKS DOWN

TABLE 2

/	FAN			• •											. 1890. . 1540. . 1440.
	i	FLOW	CFS	629	643	646	620	295	653			602	593	593 593 628	602. 593. 628. 585.
1															118.
	CUSH	PRESS	PSF	64.	.89	67.	74.	77.	70.	71.	75.		75.	75.	75. 75. 80.
/	FAN	nrag	r B	10930.	8380.	4600.	4060.	3770.	2820.	2850.	2120.		1800.	1800.	1800. 1540. 1320.
1	•	FLOW	CFS	718.	776.	646.	655.	702.	674.	690.	635.		642.	642.	642. 649. 629.
TINIT	TRUNK	PRESS	PSF	112.	119.	104.	100.	118.	123.	121.	123.		123.	123. 122.	123. 122. 123.
1	CUSH	PRESS	PSF	54.	52.	58.	53.	64.	72.	.69	78.	!	77.	77.	77. 76. 79.
`		DRAG	LR	870.	2700.	<b>8520.</b>	10380.	7870.	5940.	5800.	6320.	7100	0/40	7200.	7200. 7820.
		SPEFD	MFI	5.00	7.50	10.00	11.00	15.01	20.01	20.02	25.03	בט טב	1000	35.04	35.04 40.08
		FILE		16	30	18	31	20	CI CI	2	23	40		10 10	27

TABLE 3

TABLE 3

CALM WATER
TWO UNIT ACV TRAIN, HELICOPTER TOW
42.7 FT SPACING, TRACKS DOWN

/	FAN	DRAG	LB		.0906	5710.	4070.	3270.	3230.	3240.	2250.	2390.	2320.	1880.	1830.	1620.	1300.	1110.	1070.
2		FLOW	CFS	635.	617.	564.	559.	517.	612.	623.	575.	613.	590.	586.	.580.	613.	575.	561.	611.
UNIT	TRUNK	PRESS	PSF	109.	108.	111.	107.	102.	116.	115.	115.	114.	115.	118.	116.	116.	116.	116.	116.
!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!	СИЅН	PRESS	FSF	64.	.99	76.	72.	72.	75.	72.	78.	72.	77.	80.	79.	75.	79.	81.	75.
/	FAN	DRAG	E I		12790.	8200.	5500.	5190.	3820.	3490.	3020.	2740.	2710.	2030.	2180.	1740.	1510.	1290.	1130.
	-	FLOW	CFS	662.	773.	723.	708	752,	717.	657.	709.	654.	644.	607.	641,	626.	629.	616.	607.
TINIT-	TRUNK	PRESS	PSF	113.	121.	125.	114.	112.	117.	117.	125.	123.	124.	122.	125.	122.	123.	123.	123,
1	CUSH	PRESS	PSF	64.	55.	67.	58.	49.	61.	.69	69.	75.	78.	82.	79.	79.	79.	B1.	83.
`	•	DRAG	LB		B30.	2850.	10050.	11980.	11220.	10990.	7190.	7090.	6890.	6160.	6120.	6580.	7420.	7440.	
		SPEED	MPH	0.00	5.00	7.50	10.00	11.00	15.01	15.01	20.01	20.01	20.01	25.02	25.03	30.04	35.04	40.08	45.10
		SUN SUN		39	33	33 33	34	35	36	40	37	41	4	38	43	44	4.5	46	47

TABLE 4

4

CALM WATER
TWO UNIT ACV TRAIN, LCAC TOW
22.7 FT SPACING, TRACKS DOWN

		\		UNIT	1	/		UNIT	2	/
COSH	COSH	COSH	TR	Y N		HAN N	CUSH	TRUNK		FAN
DRAG PRESS	DRAG PRESS	PRESS	G.	ESS	FLOW	DRAG	FRESS	PRESS	FLOW	DRAG
LB PSF	LB PSF	PSF	<u>е</u> ,	'n.	CFS	LB	PSF	FSF	CFS	LB
<b>65.</b>	<b>65.</b>	65.	∓	3.	662.		65.	107.	619.	
3070. 57.	3070. 57.	57.	퓌	5.	719.	7500.	62.	113.	681.	7010.
8110. 58.	8110. 58.	58.	10	9.	652.	4690.		115.		.0609
10030. 52.	10030. 52.	52.	10	4	<b>.</b> 089	4370.	64.	115.	678.	4830.
10470. 63.	10470. 63.	63.	11		676.	4180.	72.	115.	620.	3880,
8080. 72.	8080. 72.	72.	-	1.	661.	3630.	81.	120.	593.	3240.
6150. 80.	6150. 80.	80.	7	м М	625.	2630.	64.	114.	668.	2590.
7030. 81.	7030. 81.	81.	=======================================	33.	614.	1720.	72.	114.	618.	1610.
40.08 7630. 82. 12	7630. 82.	82.	<del>-</del> -	М	<b>608</b>	1270.	71.	114.	624.	1210.
8570. 79.	8570. 79.	79.	**	0.	611.	1110.	72.	114.	616.	1070.

TABLE 5

CALM WATER
THREE UNIT ACV TRAIN, LCAC TOW
22.7 FT SPACING, TRACKS DOWN

`													
1	FAN	INRAG	Ë	9940.	6910.	5230.	4800.	4190.	4040.	3640.	2800.	2000.	1160.
3		FLOW	CFS	654.	654.	670.	654	651.	.099	653.	695.	721.	640.
UNIT	TRUNK	FRESS	FSF	111.	116.	115.	118.	118.	121.	123.	118.	122.	120.
	CUSH	PRESS	FSF	64.	.69	65.	71.	71.	73.	76.	64.	65.	74.
/	HAN	DRAG	LR		6320.	4690.	4820.	3860.	4040.	3350.	2520.	1660.	.086
2		FLOW	CFS		619.	605.	658.	615.	652.	614.	641.	638.	580.
UNIT	TRUNK	PRESS	PSF		112.	114.	118.	115.	123.	120.	116.	115.	111.
1	CUSH	FRESS	PSF	62.	70.	73.	70.	73.	75,	78.	70.	70.	74.
/	FAN	DRAG	LR	10856.	7590.	4130.	3930.	4550.		3490.	2800.	1930.	1210.
1		_	1										649.
UNIT	TRUNK	PRESS	PSF	107.	114.	102.	100.	110.		118.	125.	127.	123.
1		PRESS	PSF	46.	55.	63.	55.	46.	62.	71.	77.	78.	76.
		DRAG	LB	1190.	3830.	11130.	13670.	15840.	14950,	11220.	8840.	9890.	11780.
		SPFED	工业	2.00	7.50	10.00	11.00	12.51	13.57	15.01	20.02	30.02	44.89
		2		о. ИТ	9	61	69	82	70	64	65	99	67

TABLE 6

TABLE 6

CALM WATER
TWO UNIT ACV TRAIN, LCAC TOW
22.7 FT SPACING, TRACKS UP

/	FAN	nRAG	<u>a</u>	7010	5240.	4790.	4140.	3510.	2580.	1560.	1330.	1010.	1000.
· · · · · · · · · · · · · · · · · · ·	i	FI OW	F F S	654	649	647.	639	631.	662.	598	588.	555.	594.
TINI	TRUNK	PRESS	PSF	118.	119.	120.	119.	123.	114.	115.	116.	107.	111.
!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!	CUSH	PRESS	PSF	71.	72.	73.	74.	78.	.99	75.	78.	73.	72.
/	FAN	DRAG	LB	7390.	4460.	4430.	3930.	3340.	2490.	1650.	1410.	1370.	1190.
11		FLOW	CFS	696.	611.	688	641.	612.	590.	583.	578.	642.	619.
UNIT	TRUNK	<b>PRESS</b>	PSF	117.	107.	104.	112.	120.	124.	125.	126.	125.	127.
1	CUSH	PRESS	PSF	63.	99	51.	67.	78.	85.	87.	89.	80.	84.
`		DRAG	LR	2860,	<b>8</b> ∑8 <b>0.</b>	10366.	10740.	7710.	5660.	6310.	7260.	8450.	9040.
		SPEED	MPH	7.50	10.00	11.00	12.50	15.01	20.01	30.04	35.04	40.04	45.06
		N.C.N		72	73	74	75	76	77	78	81	80	29

PAGE 1

DAVIDSON LABORATORY

# TABLE 7-1 ACV BARGE TRAIN

15-SEF-82

THREE UNITS, LCAC TOW, 22.7 FT SPACING, TRACKS DOWN

FUN 86

	WEIGHT	5.0 30000. 1440.	LB				SEA	TERS STATE 110.0	2
	i	MEAN/RMS	OSC/BUF	FF AVG	1/3	1/	10	EXTRE	EME
TIRAG KIPS		1.445 1.251		4.24 -0.38				7.( -1.1	
LUT	1	FLOW	660. CF	SF	AN DRAG	10080.	LB		
DRIVER A	CC	0.007 0.176	26 0.60	0.44 -0.41	0.57 -0.51			0.7	
TROOF ACC	C	-0.022 0.150	21 0.60	0.41 -0.35	0.55 -0.41			0.8	
HOR ACC G,#1		-0.111 0.082		0.07 -0.29				0.1	
CUSH FRES	<b>3</b> S	62.981 6.279					·	91.3 42.9	
TRUNK FRE	ESS	111.610 9.429						154.3	37
LUT 2	2	FLOW	650. CF	SFA	N DRAG	9570.	LB		· <b>-</b>
DRIVER AC	CC	-0.001 0.164	22 0.60	0.37 -0.43	0.44 -0.54			0.5	
TROOP ACC	:	-0.012 0.150		0.39 -0.32				0.5	
HOR ACC G•#2			15 0.25	0.10 -0.26	0.14			0.1	
CUSH PRES	SS	61.947 7.295	24 24.00	80.76 45.25	92.53 40.37			117.1 38.2	2
TRUNK FRE	:SS	108.381 9.051	18 40.00	133.87 85.97	139.29 82.07			142.0 79.5	2

-0.17

111.03

156.78

73.56

17.47

		•	TR-2299		
DAVIDSON	LABORATORY	ACV E	ABLE 7-1 BARGE TRAIN		PAGE 2 15-SEP-82
RUN 86					
	SPEED ( WEIGHT 3000 DRAG 144	00. LB	F AVG	1/3	WAVE ENCOUNTERS 26 SEA STATE 2 LCG 110.0 IN 1/10 EXTREME
LUT 3	FLOW	430. CF	5FAN	DRAG	9600. LB
DRIVER AC	C -0.01	1 29 4 0.60	0.43	0.58	A 77
TROOP ACC G,#3	-0.00 0.15	5 40 8 0.45	0.35 -0.31	0.45	A 50
HOR ACC G,#3	0.08 0.07		0.32 -0.11		0.45 -0.17

C

CUSH PRESS

TRUNK PRESS

P'SF

PSF

67.220

111.469

10.838

9.797

76

56

24.00

36.00

86.05

49.33

136.54

88,95

94.05

42.51

143.87

82.87

101.71

150.96

77.89

36.59

DAVIDSON LABORATORY

## TABLE 7-2

28-0CT-82

## ACV BARGE TRAIN

THREE UNITS, LCAC TOW, 22.7 FT SPACING, TRACKS DOWN

RUN 87 , 112

WEIGH	10.0 30000. 12760.	LB				INTERS 44 STATE 2 110.0 IN
	MEAN/RMS	OSC/BUFF	AVG	1/3	1/10	EXTREME
DRAG KIPS	12.761 3.700	60 3.42	18.13 7.49	21.36 5.33	23.25 4.12	24.66 2.90
LVT 1	FLOW	616. CFS	F	AN DRAG	4230. LB-	من من من سنة مند لخد لك 100 (17
DRIVER ACC	0.001 0.186	11	0.42			0.51 -0.49
TROOF ACC G:#1	-0.008 0.154	6 0.60	0.44			0.61 -0.54
HDR ACC G:#1	-0.055 0.132	63 0.25	0.17 -0.28	0.26 -0.40	0.31 -0.51	0.34 -0.60
CUSH PRESS PSF	58.659 18.753	84 32.00	100.35 33.81	123.46 23.14	140.42 18.12	158.36 14.08
TRUNK FRESS PSF	100.739 12.695	8 48.00	130.83 64.86			139.83 54.96
LUT 2	FLOW	690. CFS	F	AN DRAG	5220. LB-	
DRIVER ACC G:#2	0.003 0.195	45 0.60	0.41	0.51 -0.57		0.97 -0.78
TROOF ACC G,#2	0.003 0.182	46 0.50	0.39	0.54 -0.44		0.79 -0.55
HOR ACC G:#2	-0.030 0.124	54 0.25	0.18	0.28 -0.34	0.35 -0.39	0.42 -0.44
CUSH PRESS PSF	59.185 16.163	87 24.00	94.43 40.04	132.64 26.17		250.44 -5.20
TRUNK PRESS PSF	111.457 11.032	38 40.00	136.01 94.29	143.93 77.73		145.88 74.13

DAVIDSON LABORATORY

TABLE 7-2

28-0CT-82

# ACV BARGE TRAIN

(Continued)

RUN 87 , 112

SFEED WEIGHT DRAG	10.0 30000. 12760.	LB			WAVE		NTERS STATE 110.0	2
ME	EAN/RMS	OSC/BUFF	AVG	-	1/3	1/10	EXTRE	ME

LVT 3	FLCW	700.	CFSFAN	DRAG	5620. LB-	
DRIVER ACC G,#3	-0.020 0.222	61 0.60	- · · <del>-</del>	0.53	0.62 -0.72	0.68 -0.81
TROOP ACC G+#3	-0.007 0.195	52 0.45	• • • •	0.58	0.70 -0.54	0.86
HOR ACC G,#3	0.036 0.133	36 0.35		0.44		0.60 -0.45
CUSH PRESS PSF	63.87 <b>5</b> 16.899	<b>54</b> 24.00		28.44 -2.99	183.79 -29.99	242.82 -34.85
TRUNK PRESS PSF	117.940 13.031	67 36.00		50.46 83.39	156.32 76.66	162.19 67.27

TABLE 7-3

28-0CT-82

## ACV BARGE TRAIN

# THREE UNITS, LCAC TOW, 22.7 FT SPACING, TRACKS DOWN

RUN 113, 88

	WEIGHT	12.5 30000. 17210.	LB		l.i		NTERS 40 STATE 2 110.0 IN
	i	MEAN/RMS	OSC/BUFF	AVG	1/3	1/10	EXTREME
DRAG KIPS		17.210 6.063	57 3.42	25.37 9.85	30.22 4.43	33.23 3.71	35.57 0.71
LUT	1	FLOW	746. CFS	FA	N DRAG	4645. LB-	
DRIVER A G•#1	CC	-0.012 0.287	29 1.00				1.33 -0.86
TROOF AC G,#1	С	0.010 0.296	33 0.90		0.76 -0.73		0.85 -1.04
HOR ACC G•#1		-0.171 0.177	69 0.25	0.10 -0.43	0.23 -0.56	0.33 -0.65	0.57 -0.67
CUSH FRE FSF	SS	52.573 8.561	28 32.00		85.83 27.76		107.53 19.55
TRUNK FR FSF	ESS	114.197 17.328	43 48.00				291.78 60.62
LUT	2	FLOW	600, CFS	FA	N DRAG	3670. LB-	
DRIVER A G,#2	cc	-0.004 0.211	38 0.60				0.76 -0.68
TROOF AC G,#2	C	0.002 0.231	49 0•50				0.72 -0.91
HOR ACC G•#2		0.063 0.179	53 0.25	0.23 -0.35	0.35 -0.51	0.48 -0.63	0.66 -0.76
CUSH FRE	: <b>S</b> S	73.732 7.986	40 24.00	98.58 63.43	110.30 49.83		117.94 32.26
TRUNK PR	ESS	112.999 13.209	39 40.00	138.87 83.84	147.46 75.56		156.33 65.27

28-0CT-82

DAVIDSON LABORATORY

TABLE 7-3
ACV BARGE TRAIN
(Continued)

I

EUN 113, 88

 SPEED
 12.5 MPH
 WAVE ENCOUNTERS
 40

 WEIGHT
 30000. LB
 SEA STATE
 2

 DRAG
 17210. LB
 LCG 110.0 IN

MEAN/RMS OSC/BUFF AVG 1/3 1/10 EXTREME

LVT 3	FLOW	580.	CFSFAN	DRAG	3660. LB-	
DRIVER ACC	-0.023	42	0.44	0.63		0.88
G,#3	0.254	0.60	-0.54	-0.67		-0.87
TROOP ACC	-0.008	52	0.38	0.50	0.61	0.78
G,#3	0.210	0.45	-0.37		-0.58	-0.70
HOR ACC	0.109	37	0.43	0.53		0.73
G,#3	0.151	0.35	-0.15	-0.26		-0.33
CUSH PRESS	76.795	26	78.57	91.76		103.04
PSF	14.366	24.00	34.85	19.82		3.79
TRUNK PRESS	114.679	52	142.10 j	.52.06	159.32	163.68
PSF	14.709	36.00	87.10	78.35	73.12	65.03

DAVIDSON LABORATORY

## TABLE 7-4

28-00T-82

### ACV BARGE TRAIN

THREE UNITS LCAC TOW, 22.7 FT SPACING, TRACKS DOWN

RUN 89 , 114						
SPEED WEIGHT DRAG	15.0 30000. 13330.	MPH LB LB		W		TERS 37 STATE 2 110.0 IN
	MEAN/RMS	OSC/BUFF	AVG	1/3	1/10	EXTREME
DRAG KIPS	13.628 5.620	50 3.42	21.07	25.34 2.66	28.23 0.96	28.91 -0.28
LVT 1	FLOW	560. CFS	F	AN IRAG	3060. LB	
DRIVER ACC G:#1	-0.011 0.387			1.36 -0.90		2.88 -1.15
TROOF ACC G,#1		44 0.90				1.19 -1.13
HOR ACC G,#1					0.49 -0.77	
CUSH FRESS FSF	85.564 16.703	66 32.00	114.74 55.42	131.33 40.13	152.50 28.60	189.64 17.60
TRUNK PRESS FISF	120.363 23.542	73 <b>48.</b> 00	173.79 83.53	211.47 60.52	251.97 47.79	307.13 35.56
LUT 2	FLQW	670. CFS	F	AN IIRAG	3610. LB-	
DRIVER ACC G,#2	0.005 0.348	52 0.60	0.66 -0.53	0.91 -0.72	1.18 -0.79	1.54 -0.85
TROOF ACC G,#2					0.90 -0.93	
HOR ACC G+#2	-0.070 0.209	65 0.25	0.24 -0.36		0.60 -0.65	
CUSH PRESS PSF	68.015 15.968	75 24.00	96.82 43.69			
TRUNK PRESS FSF	118.172 15.256			154.81 78.12	162.64 70.78	

TABLE 7-4

28-0CT-82

## ACV BARGE TRAIN

(Continued)

RUN 89 , 114

SFEED 15.0 MPH WEIGHT 30000. LB DRAG 13630. LB WAVE ENCOUNTERS 37 SEA STATE 2 LCG 110.0 IN

MEAN/RMS OSC/BUFF AVG 1/3 1/10 EXTREME

LVT 3	638. (	CFSF	AN DRAG	3498. LB-		
DRIVER ACC	-0.022	33	0.57	0.81		1.26
G,#3	0.324	06.0	-0.53	-0.68		-0.81
TROOP ACC	-0.012	57	0.48	0.70	0.88	1.06
G,#3	0.282	0•45	-0.43	-0.61	-0.70	-0.74
HOR ACC	0.133	38	0.50	0.68		1.22
G,#3	0.178	0.35	-0.13	-0.23		-0.38
CUSH FRESS	75.657	30	104.07	117.82		143.25
PSF	18.207	24.00	56.50	41.85		29.50
TRUNK PRESS	120.702	63	151.39	165.36	181.20	189.10
PSF	17.452	36.00	93.40	80.26	71.11	65.03

PAGE 1

#### DAVIDSON LABORATORY

### TABLE 7-5

28-0CT-82

## ACV BARGE TRAIN THREE UNITS, LCAC TOW, 22.7 FT SPACING, TRACKS DOWN

RUN 117 , 118

	WEIGHT	25.0 30000. 11260.	LB				NTERS 36 STATE 2 110.0 IN
		MEAN/RMS	OSC/BUF	F AVG	1/3	1/10	EXTREME
DRAG KIFS		11.258 4.335			20.55 2.73		23.81 1.51
LUT 1		FLOW	681. CF	SF	AN DRAG	2158. LB-	
DRIVER AC	CC	-0.009 0.754	50 1.00	1.70 -0.73	2.48 -1.07	2.96 -1.22	3.09 -1.60
TROOF ACC		0.022 0.550	51 0.90	1.11 -0.59	1.60 -0.89	1.89 -1.00	2.54 -1.05
HOR ACC G•#1		-0.120 0.255			0.46 -0.67		0.64 -1.10
CUSH PRES	SS	64.875 38.089	38 32.00	130.25 28.20	163.83 8.31		188.54 -21.52
TRUNK FRE	ESS	116.196 47.074	79 48.00	208.02 70.40	263.91 48.76	301.48 36.57	324.11 16.97
LUT :	<u> </u>	FLOW	635 CF	SF	AN DRAG	1947 LB	
DRIVER AG G,#2	CC	0.004 0.616			2.09 -0.93		2.58 -1.14
TROOP ACC G:#2		0.006 0.373			0.94 -0.70		1.34 -0.94
HOR ACC G;#2		-0.028 0.190	44 0+25	0.30 -0.30	0.48 -0.39		0.62 -0.54
CUSH PRES	6S	67.764 27.913	33 24.00	109.80	145.31 19.56		186.41 1.28
TRUNK PRE PSF	ESS	112.442 28.946	48 40.00	166,86 75,91			204.08 35.82

#### TABLE 7-5

28-0CT-82

### ACV BARGE TRAIN

(Continued)

RUN 117, 118

C

	25.0 T 30000. 11260.	LB				NTERS 36 STATE 2 110.0 IN
	MEAN/RMS	OSC/BUFF	F AVG	1/3	1/10	EXTREME
LVT 3	FLOW	680. CF	SFA	N DRAG	2180. LB-	
DRIVER ACC	-0.008 0.514	46	0.88 -0.58	1.36		2.03
TROOF ACC					1.06	-1.03 1.23
G, #3	0.382	0.45	-0.44	-0.66	-0.79	
HOR ACC G,#3	0.053 0.189	28 0.35	0.39 -0.28	0.51 -0.39		0.69 -0.54
CUSH PRESS PSF	67.241 25.004		100.54 35.06			124.11 -50.42
TRUNK PRESS PSF	118.075 26.594	50 36.00	163.70 85.67	189.30 69.66	208.42 58.65	219.55

28-0CT-82

TABLE 7-6

## ACV BARGE TRAIN

## THREE UNITS, LCAC TOW, 22.7 FT SPACING, TRACKS DOWN

RUN 116, 92

	WEIGHT	30.0 30000. 12490.	LB				NTERS 28 STATE 2 110.0 IN
		MEAN/RMS	OSC/BUF	F AVG	1/3	1/10	EXTREME
JRAG KIPS		12.487 4.758	23 3.42	18.43 6.25	21.66 3.42		27.77 1.59
LVT	ļ <b></b>	FLOW	603, CF	3F	AN DRAG	1540. LR-	
DRIVER AC G+#1	CC	0.010 0.783	36 1.00	1.63 -0.67	2.27 -1.07		3.04 -1.49
TROOP ACC G,#1		0.007 0.608	36 0.90	1.14 -0.59	1.48 -0.97		1.98 -1.36
HOR ACC G,#1		-0.102 0.282	28 0.25	0.32 -0.50	0.46 -0.65		0.65 -0.89
CUSH PRES		30,430	<b>3</b> 2.00	38.43	14.61	177.21 6.57	1.96
TRUNK PRE PSF	SS	112.444 45.396	32 48.00	200.27 67.74	235.35 46.80	251.36 35.36	268.34 29.10
LVT 2		FLOW	590. CFS	F	N DRAG	1510. LB	
DRIVER AC G,#2	С	-0.014 0.692	37 0.60	1.25 -0.62	1.80 -0.98		2.38 -1.06
TROOF ACC G,#2		0.003 0.415	35 0.50	0.73 -0.46	1.06 -0.72		1.43 -0.97
HOR ACC G,#2		-0.035 0.203	04 0+25	0.27 -0.31	0.38 -0.47		0.56 -0.71
CUSH PRES PSF	ទ	73.757 33.340	45 24.00	131.26 43.73	161.11 17.51		191.94 3.45
TRUNK FRE	SS	112.471 31.311	35 40.00	145.04 76.82	181.27 58.59		191.24 39.06

TABLE 7-6

28-0CT-82

EXTREME

218.70

47.84

#### ACV BARGE TRAIN

(Continued)

RUN 116, 92

TRUNK PRESS

PSF

116.740

31.739

SFEED	30.0	MPH	WAVE ENCOUNTE	S 28	
WEIGHT DRAG	30000. 12490.		SEA ST	_	
271110	127/01	LD	LCG 11	••0 IN	

1/3

192.31

61.19

1/10

----LVT 3------FLOW 694. CFS-----FAN DRAG 1842. LB-----DRIVER ACC -0.025 33 1.07 1.57 2.49 G,#3 0.635 0.60 -0.70 -1.01 -1.18 TROOP ACC -0.008 41 0.78 1.06 1.43 G,#3 0.483 0.45 -0.46 -0.85 -1.11 HOR ACC 0.070 22 0.49 0.68 0.99 G,#3 0.277 0.35 -0.34 -0.48 -0.59 CUSH FRESS 43.308 17 106.63 138.88 174.34 FSF 30.967 24.00 25.87 1.52 -10.70

167.73

80.71

MEAN/RMS DSC/BUFF AVG

35

36.00

#### TABLE 7-7

#### 28-0CT-82

#### ACV BARGE TRAIN

#### THREE UNITS, LCAC TOW, 22.7 FT SPACING, TRACKS DOWN

FUN 120 , 119

	WEIGH	35.0 30000. 14110.	LB				NTERS 31 STATE 2 110.0 IN
		MEAN/RMS	OSC/BUFF	AVG	1/3	1/10	EXTREME
DRAG KIFS		14.108 5.463	27 3.42	20.73 7.45	26.31 4.11		33.15 2.22
LVT	1	FLOW	650. CF	6F	AN IIRAG	1460. LB-	
DRIVER ANGLE	CC	-0.007 0.873	46 1.00	1.70 -0.76	2.53 -1.16		4.52 -1.64
TROOF ACC G+#1	С	0.070 0.590	39 0.90	1.14 -0.62	1.57 -0.90		2.76 -1.20
HOR ACC G,#1		-0.101 0.325					1.15 -1.27
CUSH FRES	SS	67.405 42.140	60 32.00			183.09 -17.34	
TRUNK PRI PSF	ESS	114,796 56,781	63 48.00	210.63 62.70	272.19 36.68	311.06 24.02	411.40 9.70
LUT 2	2	FLOW	570. CFS	6F	AN DRAG	1210. LB-	
DRIVER AG G,#2	CC	0.002 0.693	45 0.60	1.22 -0.63	1.92 -1.00		4.41 -1.30
TROOF ACC	C	-0.001 0.507	40 0.50	0.95 -0. <b>5</b> 1	1.53 -0.84		3.28 -1.10
HOR ACC G,#2		-0.037 0.234	42 0.25	0.28 -0.38	0.49 -0.57		0.69 -0.80
CUSH FRES	SS	72.590 33.693	49 24.00	126.83 39.41	156.96 21.69		247.48 -1.60
TRUNK PRE PSF	ESS	108.930 33.673	40 40.00	164.54 69.87	187.01 49.86		210.75 24.99

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DAVIDSON LABORATORY

SPEED

WEIGHT

#### TABLE 7-7

28-0CT-82

WAVE ENCOUNTERS

SEA STATE

#### ACV BARGE TRAIN

(Continued)

35.0 MPH

30000. LB

RUN 120, 119

CANDERSON AND DESCRIPTION OF THE PROPERTY OF T

DRAG	14110.	LB			LCG	110.0 IN
	MEAN/RMS	USC/BUFF	AVG	1/3	1/10	EXTREME
LVT 3	FLOW	630. CF	5FA	N DRAG	1440. LB-	
DRIVER ACC	-0.006	43	1.22	1.83		2.32
G,#3	0.773	0.60	0.72	-1.17		-1.53
TROOF ACC	-0.018	41	0.86	1.50		2.46
G•#3	0.630	0.45	-0.61	-1.00		-1.51
HOR ACC	0.058					1.55
G• <b>‡</b> 3	0.364	0.35	-0.43	-0.66		-1.01
CUSH PRESS	72.281	50	109.74	135.51	151.61	160.42
PSF	29.618	24.00	41.51	8.40	-14.39	-36.67
TRUNK PRESS	116.770	41	178.09	204.82		248.12
PSF	40.189	36.00	71.43	45.65		24.06

TABLE 7-8

28-0CT-82

#### ACV BARGE TRAIN

#### THREE UNITS, LCAC TOW, 22.7 FT SPACING, TRACKS DOWN

RUN 93, 121

SPEED 44.7 MPH WAVE ENCOUNTERS 26
WEIGHT 30000. LB SEA STATE 2
LB LCG 110.0 IN
MEAN/RMS OSC/BUFF AVG 1/3 1/10 EXTREME

LUT 1	C	FSF	AN DRAG	LB	
DRIVER ACC	-0.021	25	2.08	2.92	3.67
G+#1	1.004	1.00	-0.96	-1.23	-1.37
TROOF ACC	0.002	20	1.03	1.46	1.72
G,#1	0.529	0.90	-0.63	-0.91	-1.26
HOR ACC	-0.078	23	0.40	0 : 63	0.93
G+#1	0.326	0.25	-0.48	-0 : 74	-0.90
CUSH PRESS	68.089	38	136.70	179.39	202.94
PSF	44.714	32.00	29.05	1.41	-12.90
TRUNK PRESS					

		580. CI	580. CFSFAN		980. LB	
DRIVER ACC	0.014	32	1.32	2.20	3.26	
G.#2	0.786	0.60	-0.55	-1.04	-1.28	
TROOF ACC	-0.002	25	0.99	1.46	1.79	
G+#2	0.523	0.50	-0.55	-0.82	-1.07	
HOR ACC	-0.027	24	0.22	0.38	0.52	
G+#2	0.194	0.25	-0.31	-0.46	-0.73	
CUSH PRESS	72.506	38	133.31	166.68	220.89	
PSF	36.718	24.00	45.18	15.93	1.72	
TRUNK PRESS	110.244	26	169.52	198.29	218.91	
PSF	39.101	40.00	67.20	41.68	30.11	

28-0CT-82

DAVIDSON LABORATORY

TABLE 7-8

ACV BARGE TRAIN

(Continued)

RUN 93 , 121

SFEED 44.7 MPH WEIGHT 30000. LB DRAG LB

WAVE ENCOUNTERS 26 SEA STATE 2

LCG 110.0 IN

MEAN/RMS OSC/BUFF AVG 1/3 1/10 EXTREME

-----FLOW CFS----FAN DRAG LB-----DRIVER ACC -0.015 31 1.13 1.70 2.50 G, #3 0.659 0.60 -0.63 -0.94 -1.25 TROOF ACC -0.012 31 0.63 1.03 1.62 G,#3 0.424 0.45 -0.46 -0.71 -1.01 HOR ACC 0.036 7 0.36 0.62 G,#3 0.174 0.35 -0.23 -0.38 CUSH PRESS PSF TRUNK PRESS 116.539 29 170.68 190.60 214.90 PSF 32,750 36.00 78.79 55.81 41.01

C

C

r

IJ. € TABLE 8-1

16-SEF-82

#### ACV BARGE TRAIN

FOUR UNITS, LCAC TOW, 22.7 FT SPACING, TRACKS DOWN

	WEIGHT	5.0 30000. 1760.	LB				NTERS 46 STATE 2 110.0 IN
		MEAN/RMS	OSC/BUF	F AVG	1/3	1/10	EXTREME
DRAG KIPS		1.760 1.279			5.46 -0.47		6.24 -0.63
LUT 1		FLOW	640. CFS	5F	AN DRAG	9660. LB-	
TROOF ACC		-0.189 0.142	46 0.60	0.23 -0.54	0.33 -0.61		0.42 -0.78
HOR ACC G:#1		-0.078 0.082	50 0.25	0.09 -0.25	0.15 -0.29	0.19 -0.31	0.20 -0.32
F'SF		65.540 6.613	32.00	47.56	43.93		117.03 42.21
TRUNK FRE	SS	110.821 10.678	72 48.00	143.60 85.97	153.23 80.55	158.21 78.20	161.65 74.36
LUT 2		FLOW	630. CFS	F	AN DRAG	9180. LB	
DRIVER ACC	C	-0.003 0.150	68 0.60	0.34	0.40 -0.47	0.43 -0.51	0.50 -0.52
TROOP ACC G,#2		-0.016 0.141	46 0.50	0.34 -0.33	0.43 -0.42	0.49 -0.49	0.52 -0.53
HOR ACC G•#2		-0.074 0.079	40 0.25	0.11 -0.26	0.16 -0.31		0.21 -0.35
CUSH FRESS	3	63.462 5.681	24 24.00	83.82 47.70	95.65 40.17		113.21 31.76
TRUNK PRES	SS	107.210 8.180	22 40.00	132.41 85.40	135.83 82.13		137.62 77.16

16-SEF-82

DAVIDSON LABORATORY

TABLE 8-1

ACV BARGE TRAIN

(Continued)

RUN 94

TRUNK PRESS

FSF

WEIGH	5.0 T 30000. 1760. MEAN/RMS	LB LB	FF AVG		LCG	STATE 2 110.0 IN
+LUT 3	FLOW	710. C	FSFA	N DRAG 1	0890. LB	
DRIVER ACC G+#3	0.040 0.227	33 1.00	0.61 -0.56	0.71 -0.65		1.32 -0.73
CUSH PRESS PSF					90.12 25.93	
TRUNK FRESS					150.79 81.39	
LUT 4	FLOW	C	FSFA	N DRAG	LB	
	-0.023					
G• <b>*</b> 4	0.172	0.60	-0.39	-0.51	-0.64	-0.84
TROOF ACC			0.35	0.46	0.58	0.75
G• #4	0.169	0.50	-0.38	-0.50	-0.61	-0.71
	0.043					0.36
G , #4	0.076	0.40	-0.18	-0.20	-0.21	-0.21
CUSH PRESS	66.664	114	83.79	90.31	95.03	97.39
PSF	8.784	24.00	49.00	42.74	34.83	26.45

FAGE 1

DAVIDSON LABORATORY

## TABLE 8-2 ACV BARGE TRAIN

17-SEP-82

FOUR UNITS, LCAC TOW, 22.7 FT SPACING, TRACKS DOWN

	WEIGHT	10.0 30000. 15880.	LB				NTERS 48 STATE 2 110.0 IN
		MEAN/RMS	OSC/BUF	F AVG	1/3	1/10	EXTREME
DRAG KIFS		15.882 3.900	53 3.42	20.80 10.13	23.74 7.50	25.54 5.87	27.62 4.72
<del>-</del> -LVT	1	FLOW	650. CF	SF	AN DRAG	4750. LB-	
TROOF ACC		-0.033 0.264	44 1.00	0.42 -0.63	0.77 -0.76		0.89 -0.98
HOR ACC G,#1		-0.045 0.119	55 0.25	0.17 -0.25	0.24 -0.35	0.28 -0.40	0.37 -0.43
CUSH PRES	SS	59.973 18.601	81 32.00	96.29 35.16	121.88 24.20	139.80 18.29	149.26 11.51
TRUNK FRE	ESS	106.962 17.789	72 48.00	152.84 76.20	186.03 65.10	242.17 59.61	365.33 52.54
LVT 2	2	FLOW	690. CFS	6F	AN DRAG	5260. LB	
DRIVER AC G,#2	CC	0.008 0.209	57 0.60	0.43 -0.42	0.57 -0.56	0.64 -0.64	0.70 -0.68
TROOP ACC	;	-0.001 0.192	63 0.50	0.36 -0.39	0.48 -0.54	0.57 -0.62	0.67 -0.65
HOR ACC G:#2		-0.022 0.111	39 0.25	0.20 -0.23	0.27 -0.31		0.36 -0.35
CUSH PRES PSF	S	57.866 ±2.437	72 24.00	81.45 40.26	103.08 30.72	128.02 26.25	150.20 19.43
TRUNK PRE	SS	111.218 11.947	82 <b>4</b> 0.00	135.94 84.10	143.01 76.60	149.10 71.54	157.43 66.64

FAGE 2

DAVIDSON LABORATORY

# TABLE 8-2 ACV BARGE TRAIN

17-SEF-82

(Continued)

RUN	98
-----	----

	WEIGHT	10.0 30000. 15880.	LB				NTERS 48 STATE 2 110.0 IN
		MEAN/RMS	OSC/BUF	F AVG	1/3	1/10	EXTREME
LUT 3	3	FLOW	730. CF	SFA	N DRAG	5820. LB	
DRIVER AD	C	-0.009	58	0.46	0.60	0.73	0.90
0,40		0.210	0.80	-0.43	~0.57	-0.69	-0.76
TROOP ACC	;	-0.005	75 0 45	0.39	0.54	0.60 -0.57	0.70
0,10		0.208	0.43	-0.32	-0.48	-0.57	-0.68
HOR ACC G•≢3							
CUSH PRES	s	58.394	94	79.92	98.35	118.55	150.57
PSF		14.848	24.00	37.64	23.01	13.43	-17.43
TRUNK PRE	SS	117.176	108	144.29	155.10	161.79	17/ /0
PSF		13.620	36.00	92.99	83.88	78.81	66,17
LUT 4		FLOW	600. CF	SFA	N DRAG	4520. LB	
DRIVER AC							
G, #4			0.60	-0.45	U.54	0.66 -0.68	0.76
							-0.77
TROOF ACC		-0.017	59	0.39	0.55	0.67	0.76
G•#4		0.204	0.50	-0.39	-0.56	-0.68	
HOR ACC		0.042	17	0.33	0.42		0.47
G,#4		0.113	0.40	-0.22	-0.28		-0.33
CUSH PRES	S	69.113	40	00 70	00 00		
PSF		11.374		07 • 38 48 : 77	77.89	111.63 32.43	117.33
TRUNK PRE	SS		• • • •	, u , , u	30171	J 43	∠6•U/

TABLE 8-3

ACV BARGE TRAIN

PAGE 1

DAVIDSON LABORATORY FOUR UNITS, LCAC TOW, 22.7 FT SPACING, TRACKS DOWN

16-SEP-82

EXTREME

1/10

R:UN 95

SFEED 12.5 MPH WAVE ENCOUNTERS 43 WEIGHT 30000. LB SEA STATE 2 DRAG LB LCG 110.0 IN MEAN/RMS OSC/BUFF AVG 1/3

LVT 1	EL OH	700 C	FC	AN ESTAC	4/10 10	
	FLOW	/00. C	r 5	HIN TIVER	4010. LB	
IRIVER ACC	-0.010	60	0.68	0.90	1.03	1.19
G•#1	0.337	1.00	-0.72	-0.90	-0.98	-1.07
TROOF ACC	-0.019	72	0.49	0.71	0.85	1.19
G,#1	0.292	0.60	-0.52	-0.72	-0.83	-1.05
HOR ACC	-0.121	57	0.13	0.25	0.31	0.38
G,#1	0.154	0.25	-0.37	-0.48	-0.56	-0.65
CUSH FRESS	65.301	87	89.44	98.27	106.37	112.43
<b>P</b> SF	12.885	32.00	41.53	31.65	25.50	21.87
TRUNK PRESS	120.160	132	163.09	192.71	230.98	442.92
FSF	23.668	48.00	85.47	70.83	61.66	50.92
LVT 2	FLOW	580. C	FSF	AN DRAG	3520. LB-	
DRIVER ACC	0.001 0.216	65	0.41	0.56	0.68	0.75
G•#2	0.216	0.40	-0.45	-0.61	-0.72	-0.81
TROOF ACC	-0.009	95	0.38	0.59	0.74	0.88
G,#2	0.243	0.50	-0.40			
HOR ACC	-0.064	51	0.19	0.30	0.36	0.41
G, #2	0.150	0.25	-0.31	-0.41	-0.45	-0.50
CUSH FRESS	74.514	45	89.14	93.86		100.88
F'SF	5.993	24.00	59.50	55.45		50.82
TRUNK PRESS				155.68	148.30	192.50
F'SF	15.525	40.00	83.85	71.43	64.26	51.71

TABLE 8-3 ACV BARGE TRAIN DAVIDSON LABORATORY (Continued)

16-SEF-82

PAGE 2

RUN 95

F'SF

	, ,						
	WEIGHT	12.5 30000. 20470.	LB		h		NTERS 43 STATE 2 110.0 IN
		MEAN/RMS	OSC/BUF	F AVG	1/3	1/10	EXTREME
LUT	3	FLOW	710. CF	5F	AN DRAG	4350. LB	
DRIVER G•#3	ACC	0.012 0.276	116 0.60	0.48 -0.44	86.0 86.0-	0.83 -0.84	1.09 -0.96
CUSH FR	ESS	57.740	80	79.94	89.97	95.84	117.29
PSF		12.790	24.00	42.62	29.20	18.03	-21.00
TRUNK P FSF	RESS	113.056 16.588	163 36.00	141.00 89.57	154.21 77.44	162.29 70.43	175.65 59.06
						3310. LB	P the rate and rate the pay and
DRIVER	ACC :	0.001	64	0.47	0.64	0.76	0.92
G • #4		0.249	0.60	-0.46	-0.61	-0.72	-0.78
TROOP A	רר						
G • #4		0.235	0.50	0.40	0.60	0.81	0.98
		V+255	0.30	-0.39	~0.53	-0.63	-0.76
HOR ACC		0.099	22	0.46	0.61		0.94
G , #4		0.149	0.40	-0.17	-0.26		
CUSH PR	ESS	69.343	90	00 07	05 4 4	100 -	
F'SF		12.434	24.00	48.45	75.16 36.10	100.84 25.54	103.53
			- • • •	,0,,,0	30 • 17	£U+U4	12.60
TRUNK PI	RESS						

FAGE 1

DAVIDSON LABORATORY

## TABLE 8-4

#### ACV BARGE TRAIN

17-SEF-82

FOUR UNITS, LCAC TOW, 22.7 FT SPACING, TRACKS DOWN

	WEIGHT	12.5 30000. 20470.	LB				NTERS 42 STATE 2 110.0 IN
	i	MEAN/RMS	OSC/BUFF	F AVG	1/3	1/10	EXTREME
DRAG KIFS		22.353 6.322		30.98 14.27			39.03 3.89
LVT 1	l	FLOW	730. CFS	6FAN	DRAG	4560. LB	~
DRIVER AC G+#1	CC	-0.011 0.318	48 1.00	0.67 -0.70	0.87 -0.84		1.01 -0.99
TROOF ACC		0.032 0.351	95 0.90	0.69 -0.61	0.89 -0.89	1.02 -1.07	1.32 -1.28
HOR ACC G∙#1		-0.117 0.155	52 0.25	0.14 -0.39	0.24	0.32 -0.57	0.43 -0.59
CUSH FRES PSF	SS						
TRUNK FRE	: <b>s</b> s	113.776 18.193	64 48.00	159.22 83.22	183.84 71.53	221.23 62.70	341.89 54.96
LUT 2		FLOW	620. CFS	FAN	DRAG	3780. LR	
DRIVER AC				0.43 -0.43			0.91 -0.64
TROOF ACC		-0.002 0.227	56 0.50	0.42 -0.40	0.56 -0.55	0.66 -0.63	0.72 -0.66
HOR ACC G,#2		-0.026 0.162	53 0 - 25	0.23 -0.28	0.33	0.41 -0.48	
CUSH PRES	:5	68.277 8.358	44 24.00	86.65 50.95			99.01 40.35
TRUNK PRE	SS	111.299 13.189	41 40.00	138.80 82.34	146.13 75.50		158.27 70.80

TABLE 8-4
ACV BARGE TRAIN
(Continued)

17-SEP-82

KUN	75

C

SF We Dr	PEED 12.5 HIGHT 30000. RAG 20470.	MFH LB LB				NTERS 42 STATE 2 110.0 IN
	MEAN/RMS	OSC/BUFF	` AVG	1/3	1/10	EXTREME
LVT 3	FLOW	730. CFS	F	AN DRAG	4620. LB-	
DRIVER ACC	-0.016	42	0.46	0.63		0.85
G,#3	0.246	0.60	-0.51	-0.65		-0.81
TROOF ACC	-0.007	65	0.37	0.53	0.64	C.74
G,#3	0.231	0.45	-0.39	-0.59	-0.78	-0.99
HOR ACC G,‡3						
CUSH PRESS PSF						
TRUNK PRESS	115.334	56	141.10	148.44	153.01	157.14
PSF	13.349	36.00	89.84	81.56	75.31	69.17
LUT 4	FLOW	CFS	FA	N DRAG	LB	
DRIVER ACC	-0.007	45	0.47	0.65		0.92
G,#4	0.241	0.60	-0.45	-0.60		-0.81
TROOF ACC	-0.014	53	0.44	0.45	0.84	1.02
G,#4	0.235	0.50	-0.39	-0.55	-0.65	-0.70
HOR ACC	0.037	26	0.38	0.54		0.87
G,#4	0.157	0.40	-0.23	-0.33		-0.45
CUSH FRESS	68.461	55	87.59	94.08	98.35	101.23
PSF	11.311	24.00	47.71	38.08	31.44	25.69
TRUNK PRESS						

#### TABLE 8-5

#### ACV BARGE TRAIN

17-SEF-82

FOUR UNITS, LCAC TOW, 22.7 FT SPACING, TRACKS DOWN

	WEIGH	15.0 T 30000. 17820.	LB				NTERS 42 STATE 2 110.0 IN
		MEAN/RMS	OSC/RUFF	AVG	1/3	1/10	EXTREME
DRAG KIPS		17.816 7.446	54 3.42	24.54 7.94	31.90 2.78	34.57 -1.35	37.67 -6.56
LVT 1		FLOW	CFS	F	AN DRAG	LB-	
DRIVER AC		-0.005 3.421					2.03 -1.45
TROOF ACC	:						
HOR ACC G,#1		-0.113 0.231	47 0.25		0.40		0.79 -0.77
CUSH PRES	SS	66.317 16.646	57 32.00	96.51 39.02	110.65 26.56	128.80 17.84	145.81 9.98
TRUNK FRE	SS						
LUT 2	?	FLOW	670. CFS	F	AN DRAG	3810. LB-	
DRIVER AC	C	-0.001 0.336	42 0.60				1.30 -0.85
TROOF ACC		-0.007 0.318	<b>45</b> 0.50				1.02 -0.93
HOR ACC G,#2		-0.069 0.242	47 0.25				0.76 -1.03
CUSH FRES	S					120.75 23.04	
TRUNK FRE	ESS	124.598 17.166		159.40 94.28	171.06 83.20	180.76 77.80	

TABLE 8-5

17-SEF-82

## ACV BARGE TRAIN

(Continued)

RU	N	1	0	0

FSF

SPEEI Weich Drag	15.0 T 30000. 17820.	LB FB WE:H				NTERS 42 STATE 2 110.0 IN
	MEAN/RMS	OSC/BI	UFF AVG	1/3	1/10	EXTREME
LVT 3	FLOW	640.	CFSFAN	DRAG	3480. LB-	
DRIVER ACC	-0.010	37	0.73	1.03		1.58
6, \$3	0.382	0.40	0.73 -0.56	-0.85		-1.15
						•
TROOP ACC	-0.014	53	0.47	0.73	0.84	0.95
G, \$3	0.334	0.45	-0.50	-0.76	-0.98	
HOR ACC G, (3					2772	1135
CUSH PRESS	77.400	40	00 50	115 70	400	
PSF	18.877	24.00	45.93	112.37	128.61	137.89
TRUNK FRESS	119.279	51	155.27	168.51	177.82	189.72
F'SF	19.421	36.00	91.76	77.09	69.17	67.67
			-			0,.0,
6 11 <del>79</del> - A						
LUT 4	FLOW	C	FSFAN	DRAG	LB	
DRIVER ACC	0 004	76	0.63			
G, #4	0.008	0.40	-0.51	0.84		1.15
<b>4.4</b>	V•321	0.60	-0.51	-0./1		-0.92
TROOP ACC	-0.015	37	0.49	0 71		4 04
G+#4		0.50	-0.50	~0.4P		1.06 -0.99
						-0.99
HOR ACC	0.125	28	0.53	0.70		0.89
G , #4	0.202	0.40	-0.18	-0.30		-0.50
CHOM PRESS	04.04.5					
CUSH FRESS PSF	84.014	50	104.75	112.46	118.94	124.62
rar	14.636	24.00	61.04	48.65	40.57	30.67
TRUNK PRESS						

#### TABLE 8-6

28-0CT-82

#### ACV BARGE TRAIN

FOUR UNITS, LCAC TOW, 22.7 FT SPACING, TRACKS DOWN

RUN 101 , 108

Į.	WEIGH1	20.0 30000. 14240.	LB				NTERS 42 STATE 2 110.0 IN
		MEAN/RMS	OSC/BUFF	F AVG	1/3	1/10	EXTREME
DRAG KIPS		14.241 5.515	45 3.42	21.21	25.31 3.57		29.39 0.05
LVT 1-	~~	FLOW	669. CFS	6F	AN DRAG	2822. LB-	
DRIVER ACC G,#1	C	-0.016 0.636	65 1.00	1.32 -0.77	2.19 -1.12	3.09 -1.25	3.54 -1.30
TROOF ACC G,#1		0.041 0.417	69 0.90	0.89 -0.58	1.17 -0.84	1.38 -1.00	1.73 -1.24
HOR ACC G:#1		-0.099 0.241	<b>56</b> 0.25	0.26 -0.43	0 <b>.45</b> -0.56	0.56 -0.66	0.68 -0.81
CUSH PRESS PSF	5	74.132 28.641	91 32.00	122.43 42.35	151.76 23.90	182.10 11.30	199.81 2.74
TRUNK PRES	<b>8</b> 8	123.719 35.961					312.79 47.69
LVT 2-		FLOW	740. CFS	6F	AN DRAG	2790. LB-	
DRIVER ACC G:#2	C	0.003 0.507	52 0.60	0.89 -0.64	1.42 -0.93	1.89 -1.06	2.71 -1.30
TROOF ACC 6,#2		0.007 0.347	53 0 <b>.5</b> 0	0.55 -0.53	0.82 -0.75	0.96 -0.85	1.06 -0.95
HOR ACC G•#2		-0.052 0.234	47 0.25	0.31 -0.41	0.47 -0.59		0.92 -0.85
CUSH PRESS PSF	3	49.820 33.716	71 24.00	88.02 15.90	116.95 -25.44		218.82 -59.96
TRUNK PRES	35	110.656 21.469	53 40.00	152.89 77.77	169.88 63.63		199.08 51.65

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DAVIDSON LABORATORY

TABLE 8-6
ACV BARGE TRAIN
(Continued)

RUN 101 , 108

		•								
•		WEIGHT		LB		ţ	JAVE	SEA	NTERS 4	2
•		DRAG	14240.	LB				LCG	110.0	.N
•			MEAN/RMS	OSC/B	UFF AVG	1/3		1/10	EXTREM	1E
(	•									
• `	LVT 3		FLOW	775	CFS	FAN DRAG	303	7 LB-		_
€.	DRIVER AC	С	-0.028	39	0.87	1.35			2.14	1
	G,#3		0.451	0.60	-0.64	-0.88			-1.01	
C	TROOP ACC		-0.003	45	0.47	0.73			1.29	)
0	G+#3			0.45		-0.54			-0.70	)
C	HOR ACC		0.022	15	0.28	0.38			0.49	,
	G,#3				-0.30				-0.42	
0	CUSH PRES	S	48.516	19	90.73	131.14			172.35	
•	PSF				11.56				-59.55	
C	TRUNK FRE	SS	114,997	48	158.52	183.22			214.29	,
	PSF		23.803	36.00	81.58	65.98			55.64	}
_ (·	LUT 4		ELOU	712	CEC	TAN DEAC	2611	1 15 ~		_
				1 1 3	Cr 5	HIA DKHG	2044	CP		_
C	DRIVER AC	C			0.76				1.20	
	G,#4		0.483	0.60	-0.72	-0.99			-1.28	3
C	TROOP ACC		-0.012	32	0.59	0,92			1.38	5
<b>(</b>	G,#4		0.291	0.50	-0.46	-0.66			-0.79	7
C	HOR ACC		0.059	28	0.41	0.57			0.87	7
	G • #4		0.184	0.40		-0.35			-0.46	
•	CUSH PRES	S	52.530	38		108.38			148.49	
•	PSF		27.019	24.00	9.28	-24.55			-62.75	5
£.	TRUNK PRE	SS	108.825			156.20			179.8	7
	FSF		34.953	36.00	38.90	-31.92			-88.7	6

TABLE 8-7

20-SEF-82

EXTREME

#### ACV BARGE TRAIN

FOUR UNITS, LCAC TOW, 22.7 FT SPACING, TRACKS DOWN

**F:UN** 105

SPEED 25.0 MPH WAVE ENCOUNTERS 21 WEIGHT 30000. LE SEA STATE 2 IIRAG LB LCG 110.0 IN MEAN/RMS OSC/BUFF AVG

1/3

1/10

----LVT 1-----FLOW 650. CFS----FAN DRAG 2120. LR-----DRIVER ACC -0.026 25 1.70 2.48 3.34 G,#1 0.781 1.00 -0.81 -1.10 -1.26 TROOP ACC 0.007 24 1.06 1.46 1.56 G, #1 0.556 0.90 -0.60 -0.93 -1.00 HOR ACC -0.086 21 0.36 0.53 0.77 G, #1 0.25 0.286 -0.47 -0.67 -0.96 CUSH FRESS 71.018 36 131.69 161.52 184.65 F'SF 35.114 32.00 34.22 11.91 -37.18 TRUNK FRESS 118.541 37 205.84 253.73 297.43 FSF 44.161 48.00 74.58 54.96 40.41 -----------------------FL.OW 660. CFS----FAN IRAG 1910. LB----DRIVER ACC 0.002 26 1.31 2.01 2.79 G,#2 0.647 0.60 -0.66 -0.89 -1.03TROOF ACC 0.002 23 0.76 1.14 1.75 G - #2 0.434 0.50 -0.52 -0.75 -1.03 HOR ACC -0.066 23 0.25 0.49 0.76 G, #2 0.240 0.25 -0.29 -0.53 -0.75 CUSH FRESS 57.798 38 112.27 152.22 218.39 F'SF 33.088 24.00 27.63 3.52 -72.90 TRUNK FRESS 106.022 26 160.35 178.35 202.42 F'SF 28.185 40.00 70.68 57,20 44.98

TABLE 8-7

20-SEF-82

## ACV BARGE TRAIN (Continued)

SPEEI WEIGH DRAG	25.0 IT 30000.	FB FB Weh			WAVE	SEA	NTERS STATE 110.0	2
	MEAN/RMS	OSC/BU	FF AVG	1/3	-	1/10	EXTRI	EME
LUT 3	FLOW	650. CF	FSFA	N DRAG	2070	• FB		
DRIVER ACC	-0.015	26	0.91	1.34			1.	77
G,#3	0.541	0.60	-0.58	-0.91			-1.3	
TROOP ACC								- ,
TROOF ACC G,#3	-0.011	25	0.54	0.83			1.	18
0743	0.381	0.45	-0.46	-0.76			-1.	10
HOR ACC	0.006	17	0.41	A (A				
G • #3	0.274	0.35	0.41 -0.43	-0.62			0.7	
							-0.8	36
CUSH PRESS	71.843	38	112.23	139.07			190.8	) <del>-</del>
PSF	31.139	24.00	44.74	19.80			-89.5	
TEUNE DEECC							G / • •	
TRUNK FRESS FSF	117,961	27	165.91	187.13			205.2	26
7 37	27.645	36.00	84.66	67.67			50.3	38
LUT 4	FLOW	CF	SFA	N DRAG	LB			
DRIVER ACC G,#4	-0.005	20	1.14	1.81			3.1	1
0,44	0.600	0.60	-0.75	-0.99			-1.1	3
TROOP ACC	-0.014	10	A 74					
G • #4	0.378	0.50	-0.51	1.16			1.5	
		0.30	-0.51	-0.66			-0.7	2
HOR ACC		13	0.52	0.68			Λ. σ	
G• <b>#</b> 4	0.226	0.40	-0.31	-0.44			0.8	
OHOU DEMAN							-0.2	
CUSH PRESS FSF	69.207	22	104.95	119.02			132.7	4
r <b>3</b> r	24.232	24.00	36.87	16.00			-20.2	
TRUNK PRESS PSF								

#### TABLE 8-8

28-0CT-82

#### ACV BARGE TRAIN

FOUR UNITS, LCAC TOW, 22.7 FT SPACING, TRACKS DOWN

RUN 109 , 102

	WEIGH	30.0 30000. 14930.	LB		i		NTERS 30 STATE 2 110.0 IN
		MEAN/RMS	OSC/BUFF	AVG	1/3	1/10	EXTREME
DRAG KIPS						24.39 7.01	
LVT	1	FLOW	710. CFS	6F	AN DRAG	2000. LB-	
DRIVER A	CC	0.001 0.792	53 1.00	1.65 -0.77	2.56 -1.15	3.04 -1.29	3.26 -1.39
TROOF AC G,#1	С	-0.003 0.552	24 0.90				1.94 -1.03
HOR ACC G,#1		-0.064 0.237					0.68 -0.79
CUSH FRE PSF						168.03 3.35	
TRUNK PR PSF	ESS					314.14 38.98	
LVT	2	FLOW	600. CF	6F	AN DRAG	1530. LB-	
DRIVER A G:#2		0.013 0.637	58 0.60	1.08 -0.62	1.71 -0.97	2.26 -1.13	2.91 -1.27
TROOF AC G,#2		-0.001 0.404	46 0.50	0.74 -0.48	1.06 -0.73		1.34 -0.89
HOR ACC G:#2		-0.033 0.165	46 0.25	0.23 -0.27	0.35 -0.35		0.57 -0.48
CUSH FRE	SS	72.103 27.757	63 24.00	118.02 42.92	153.99 23.48		211.93 6.55
TRUNK PR	ESS	112.231 27.993	52 40.00	159.39 76.38	178.77 59.88		205.75 46.65

## TABLE 8-8

28-0CT-82

## ACV BARGE TRAIN (Continued)

RUN 109,102

<u></u>	SFEE Weig Drag	HT 30000.	LB			WAVE ENCOUNTERS 30 SEA STATE 2 LCG 110.0 IN
Ĺ		MEAN/RMS	OSC/BUFF	AVG	1/3	1/10 EXTREME
Ĺ	LVT 3	FLOW	640, CFS	6F	AN DRAG	1680. LB
(	DRIVER ACC G•#3	0.004 0.557	48 0.60	0.96 -0.62	1.47 -0.92	1.91 -1.14
C	TROOP ACC G, \$3	-0.006 0.334	39 0 • 45	0.57 -0.42	0.78 -0.60	1.03 -0.79
C	HOR ACC G+#3	0.017 0.212	15 0.35	0.36 -0.31	0.50 -0.42	0.83 -0.54
O	CUSH FRESS FSF	71.031 15.155				149.21
C	TRUNK FRESS PSF	115.997 24.299	46 36+00	159.02 85.93	179.04 72.32	202.24
(	LUT 4					1478 LB
(		-0.003		0.90		2.07
•	TROUP ACC	-0.041 0.315	42 0.50	0.53		1.58
Ĺ	HOR ACC G,#4	0.048 0.135	14	0.32		0.43
C	CUSH PRESS PSF	68.941 21.322	20	99.13	113.02 24.94	
<b>€</b>	TRUNK PRESS	108.658	40	148.06	195.19	
,		751200	39.00	774/7	-2/.44	-80.90

#### TABLE 8-9

#### 28-0CT-82

#### ACV BARGE TRAIN

FOUR UNITS, LCAC TOW, 22.7 FT SPACING, TRACKS DOWN

RUN	106	111	

	_						
	SPEED WEIGHT DRAG	34.8 30000. 17770.	MFH LB LB		1		NTERS 29 STATE 2 110.0 IN
		MEAN/RMS	OSC/BUF	F AVG	1/3	1/10	EXTREME
DRAG KIPS		17.768 6.026		25.11 11.15			35.82 5.15
L	VT 1	FLOW	570. CF		AN DRAG	1240. LB-	
DRIVE 6,#1		-0.003 0.899		1.86 -0.84			4.34 -1.37
TROOF G,#1	ACC	0.010 0.589	43 0.90	1.05 -0.66	1.51 -0.98	·	2.04 -1.19
HOR A G,#1	cc	-0.037 0.339	39 0.25	0.47 -0.50	0.67 -0.73		0.86 -0.94
CUSH F'SF	P'RESS	76.030 39.910	61 32.00	137.54 42.50	172.97 10.26	190.05 -3.59	206.11 -39.76
TRUNK FSF	PRESS					314.98 28.06	
<u>L</u>	VT 2	FLOW	640. CF		AN DRAG	1350. LR-	e ur filter ulder vom dem dem beste dere
DRIVE G:#1	R ACC			1.29 -0.69			2.49 -1.35
TROOF G+#2	ACC	-0.003 0.518	38 0.50	0.83 -0.56	1.25 -0.90		1.88 -1.07
HOR A G,#2	CC	-0.058 0.229	38 0.25	0.29 -0.39	0.44 -0.53		0.64 -0.62
CUSH FSF	PRESS	62.992 33.416	48 24.00	118.78 30.62	149.82 9.41		181.29 -9.59
TRUNK PSF	PRESS	108.214 35.541	40 40.00	164.58 67.49	188.97 45.04		213.24 21.66

TABLE 8-9
ACV BARGE TRAIN

28-0CT-82

(Continued)

RUN 106, 111

WEIGH	34.8 T 30000. 17770.	LB		i		NTERS 29 STATE 2 110.0 IN
	MEAN/RMS	OSC/BUF	F AVG	1/3	1/10	EXTREME
LVT 3	FLOW	618, CF		AN DRAG	1428. LB-	
DRIVER ACC G,#3	0.003 0.688	40 0.60	1.18 -0.69	1.89 -1.04		3.06 -1.13
TROOP ACC G+#3	-0.007 0.443	43 0.45	0.67 -0.49	1.03 -0.76		1.55 -0.99
HOR ACC G•#3	0.020 0.335					0.93 -0.92
CUSH PRESS PSF	75.600 37.514	23 24.00	131.57 33.74	162.92 9.62		206.75 -1.48
TRUNK PRESS PSF	117.932 32.802	39 36.00	170.62 79.08	196.70 59.40		218.05 45.86
LVT 4	FLOW	623. CF	SF	AN DRAG	1329. LB-	
DRIVER ACC G•#4	0.006 0.819	21 0.60	1.43 -0.66	2.15 -1.25		2.73 -1.38
TROOFCC G•#4	-0.039 0.592	77 3	0.97 -0.65	1.49 -1.01		1.89 -1.13
HOR ACC G,#4	0.008	21 0.40	0.54 -0.46	0.77 -0.69		0.98 -1.00
CUSH PRESS PSF	66.032 3(.863	39 24.00	107.54 33.35	141.27 14.84		205.25
TRUNK PRESS PSF	108.975 40.898		150.44 51.79			267.06 -61.27

DAVIDSON LABORATORY

#### TABLE 8-10

#### 28-0CT-82

#### ACV BARGE TRAIN

FOUR UNITS, LCAC TOW, 22.7 FT SPACING, TRACKS DOWN

RUN 110 , 107

SPEED 44.7 MFH WEIGHT 30000. LB DRAG LB

WAVE ENCOUNTERS 25 SEA STATE 2 LCG 110.0 IN

MEAN/RMS OSC/BUFF AVG

1/3 1/10 EXTREME

LVT 1	FLOW	650.	CFSF4	N TIPAC	1000 15	
				IV DIVING	1080. FR	
DRIVER ACC	-0.008	35	2.23	3.28		
G,#1	1.041	1.00	-0.88	-1.25		4.09
				-1.0		-1.48
TROOF ACC	-0.006	29	1.17	1.62		
G•#1	0.626	0.90	-0,69	-1.03		2.2
			• • • • • • • • • • • • • • • • • • • •	1.03		-1.25
HOR ACC	-0.044	35	0.44	0 41		
G• <b>+</b> 1	0.340	0.25	-0.45	-0.73		0.85
			V.75	-0./3		-1.26
CUSH FRESS	62.188	46	130.44	172.30		
PSF .	43.813	32.00		-6.24		199.61
			21170	70+24		-25.15
TRUNK PRESS	109.011	54	212.36	701 07	747	<b></b>
PSF				301.77	343.37	
			57.51	30.22	19.40	15.36
LUT 2	FLOW	610.	CFSFAN	J TIEVAG	970 15	
				. 211110	770. LB-	
DRIVER ACC	0.006	36	1.70	7 70		
G, #2	0.872	0.60	-0.74	֥/0 1 1/		4.14
			0.74	-1.10		-1.42
TROOF ACC	-0.006	39	1.01	1 55		_
G•#2		0.50	-0.53			2.20
	· -	0.00	-0+33	-0.78		-0.96
HOR ACC	-0.048	35	0.29	A = 1		
G,#2	0.257	0.25		0.51		0.96
		0120	-0.38	-0.56		-0.76
CUSH FRESS	64.346	48	123.77	4 / / ** 4		
PSF	38,921	24.00		166.31		203.04
		1+00	21.00	6.69		-11.51
TRUNK FRESS	105.158	30	175.37	105 00		
PSF	40,271	40.00				213,24
		.0.00	03+20	37.48		19.99

## TABLE 8-10 ACV BARGE TRAIN

28-0CT-82

(Continued)

RUN 110 , 107

	44.7 T 30000.	LB				NTERS 25 STATE 2 110.0 IN
	MEAN/RMS	OSC/BL	IFF AVG	1/3	1/10	EXTREME
LVT 3	FLOW	642 (	CFSF	AN DRAG	1145. LR-	
DRIVER ACC G,#3	0.023 0.618	22 0.60	1.03	1.50 -0.96		1.86 -1.29
TROOP ACC G•#3	0.004 0.447	36 0.45	0.83 -0.46	1.22 -0.70		1.97 -0.96
HOR ACC G,#3	-0.004 0.268	24 0.35	0.39 -0.42	0.63 -0.64		0,95 -0,82
CUSH PRESS PSF	71.230 41.951		135.38 30.83			210.45
TRUNK PRESS PSF	116.916 35.375	40 36.00	171.99 78.44	193.93 52.79		209.02 29.32
LVT 4	FLOW	600. C	FSF	AN DRAG	1000. LB	
DRIVER ACC G,#4						
TROOP ACC G,#4	-0.047 0.544	33 0.50	0.87 -0.61	1.44		2.64 -1.15
HOR ACC G,#4	0.026 0.258	16 0.40	0.43 -0.45	0. <b>5</b> 7		0.77 -1.13
CUSH PRESS		31	114.08	134.43		179.49
TRUNK FRESS PSF	108.416 54.359	55 36.00	167.75 46.30	229.81 -14.97	262.87 -52.89	

DAVIDSON LAROPATORY

#### TABLE 9-1

22-SEF-82

#### ACV BARGE TRAIN

#### FOUR UNITS, LCAC TOW, 13.3 FT SPACING, TRACKS DOWN

	WEIGHT	5.0 30000. 1670.	LB		WA	SEA	NTERS 77 STATE 2 110.0 IN
	i	MEAN/RMS	OSC/BUFF	AVG	1/3	1/10	EXTREME
DRAG KIPS		1.673 1.341	39 3.42	4.65 0.02	5.79 -0.18		7.55 -0.53
LUT	1	FLOW	700. CFS	F	AN DRAG 10	630. LB-	
DRIVER A G,#1	CC	-0.011 0.180					0.97 -0.69
TROOF AC		0.003 0.141	<b>4</b> 0.90	0.72 -0.39			0.76 -0.44
HOR ACC G,#1		-0.066 0.082			0.21 -0.28		0.28 -0.33
CUSH PRE PSF	SS	58.316 11.357	42 32.00	93.43 35.96	122.29 26.07		181.94 11.07
TRUNK PR PSF	ESS	112.052 12.650	72 48.00	158.94 87.25	185.93 79.11	226.11 71.73	306.32 60.62
LVT	2	FLOW	620. CFS	3F	AN DRAG 9	420. LB-	
DRIVER A					0.44 -0.45		
TROOF AC					0.46 -0.33		
HOR ACC G:#2		-0.100 0.084	46 0.25	0.12 -0.28	0.21 -0.35		0.49 -0.48
CUSH FRE FSF	:55	67.627 5.446	19 24.00	87.86 53.75	95.79 47.46		109.03 43.80
TRUNK PR PSF	ESS	110.765 6.997	8 40.00	137.96 93.29			143.27 90.80

22-SEP-82

DAVIDSON LABORATORY

TABLE 9-1 ACV BARGE TRAIN

(Continued)

WEIGH	5.0 T 30000. 1670.	LB				NTERS 77 STATE 2 110.0 IN
	MEAN/RMS	OSC/RUFF	F AVG	1/3	1/10	EXTREME
LUT 3	FLOW	680. CF9	3FAN	DRAG	10660. LB	
DRIVER ACC	-0.011	45	0.37	0.47	0.56	0.65
G,#3	0.159	0.60	-0.39		-0.56	-0.62
TROOP ACC	-0.002	63	0.33	0.40	0.45	0.54
G,#3	0.135	0.45	-0.27	-0.35	-0.42	-0.50
HOR ACC	0.074	31	0.33	0.42		0.54
G,#3	0.085	0.35	-0.16	-0.24		-0.53
CUSH PRESS	64.591	37	81.92	89.14		92.09
PSF	8.525	24.00	43.88	25.24		-33.29
TRUNK FRESS PSF	115.439 6.667	10 36.00	137.44 96.92			142.11 92.48
LUT 4	FLOW	630. CFS	3FAN	DRAG	9590. LB	
DRIVER ACC	-0.004	53	0.40	0.48	0.54	0.67
G,#4	0.162	0.60	-0.38		-0.50	-0.55
TROOF ACC	-0.002	52	0.37	0.46	0.57	0.72
G:#4	0.147	0.50	-0.29	-0.37	-0.45	-0.51
HOR ACC G,#4	0.074 0.070	4	0.34 -0.18			0.42 -0.20
CUSH PRESS	67.487	84	84.63	90.20	93.95	97.47
PSF	8.329	24.00	51.00	45.54	41.87	38.83
TRUNK PRESS	111.549	87	136.68	1 <b>44.53</b>	151.25	159.45
PSF	10.450	36.00		84.10	80.47	76.98

TABLE 9-2

22-SEF-82

#### ACV BARGE TRAIN

## FOUR UNITS, LCAC TOW, 13.3 FT SPACING, TRACKS DOWN

**RUN 124** 

	WEIGHT	10.0 30000. 12160.	LB				NTERS 44 STATE 2 110.0 IN
		MEAN/RMS	OSC/RU	FF: AVG	1/3	1/10	EXTREME
DRAG KIFS		12.160 2.964	46 3.42	16.52 7.97	18.62 6.13		23.43 4.77
LVT	1	FLOW	620. C	FSF4	AN DRAG	4160. LR	
DRIVER A	CC	-0.013 0.182	20 0.60	0.39 -0.42	0.48 -0.52		0.55 -0.60
TROOF ACC	C	0.005 0.153	14	0.38 -0.37	0.45 -0.45		0.49
HOR ACC G,#1		-0.045 0.095	42 0.25	0.15 -0.22	0.22 -0.29		0.29 -0.45
CUSH PRES		56.456 19.082	38 32.00	100.61 33.03	123.47 22.44	143.5/ 16.30	174.19 8.49
TRUNK PRE PSF	ESS	98.740 14.374	33 48.00	146.61 72.52	177.81 63.19		301.48 58.19
LVT 1	?	FLOW	630. CI	FSFA	N DRAG	4930. LB	· · · · · · · · · · · · · · · · · · ·
DRIVER AC G:#2	CC	0.006 0.210	35 0.60	0.42 -0.47	0.53 -0.60		0.66 -0.66
TROOF ACC G+#2	2	0.000	40 0.50	0.40 -0.35	0.52 -0.44		0.67 -0.56
HOR ACC G+#2		-0.049 0.091	42 0.25	0.13 -0.23	0.18 -0.30		0.22 -0.44
CUSH FRES	S	71.326 8.291	35 24.00	86.50 53.52	90.75 48.17		93.69 39.65
TRUNK FRE	SS	115.079 8.214	7 40.00	139.23 38.53			154.94 82.47

## TABLE 9-2 ACV BARGE TRAIN

22-SEP-82

(Continued)

TUN 124

	WEIGHT	10.0 30000. 12160.	LB				NTERS 44 STATE 2 110.0 IN
	٣	1EAN/RMS	OSC/BUF	F AVG	1/3	1/10	EXTREME
LUT 3		FLOW	650. CF	SF	AN DRAG	5240. LR-	
DRIVER ACI	С	0.009	33	0.45 -0.44	0.57 -0.56		0.79
TROOF ACC		-0.006	54	0.33	0.47	A 57	A 50
G+#3		0.185	0.45	~0.33	-0.44	-0.51	-0.55
HOR ACC		0.064	23	0.29	0.34		0.45
G•#3				0.29 -0.19			-0.40
CUSH PRESS	3	72.574	17	88.50	97.58		1.03.93
#SF		7.661	24.00	44.69	26.26		-13.31
TRUNK PRES	35	118.882	17	141.44	146.87		154.89
PSF		9.136	36.00	96.55	92.73		90.23
L.VT 4-		FLOW	620. CF	SFA	N DRAG	4890. LB	
DRIVER ACC	<b>-</b>	-0.013	3	0.37			0.46
G•#4		0.111	0.60	-0.72			-0.77
TROOP ACC		-0.042	31	0.38	0.50		0.76
G, #4		0.196	0.50	-0.38	-0.52		-0.71
HOR ACC		0.080	15	0.37	0.44		0.56
G•#4		0.100	0.40	-0.16	-0.22		-0.31
CUSH PRESS	3	2.177	42	90.09	97.25		105.40
F'5)		9.955	24.00	51.61	42.34		30.11
TRUNK FRES	88	115.169	51	139.80	148.13	153.56	141 00
PSF		12.474	36.00	90.38	82.89	79.20	76.19

FAGE 1

TABLE 9-3
DAVIDSON LABORATORY

### ACV BARGE TRAIN

22-SEF-82

FOUR UNITS, LCAC TOW, 13.3 FT SPACING, TRACKS DOWN

**RUN 125** 

PERSONAL PROPERTY PROPERTY OF STATES OF STATES AND STAT

WE	PEED 12.9 SIGHT 30000 RAG 14180	· LB				NTERS 38 STATE 2 110.0 IN
	MEAN/RMS	OSC/BUFF	AVG	1/3	1/10	EXTREME
DRAG	1 <b>4.</b> 177	49	20.30	23.43		27.19
KIPS	<b>4.4</b> 80	3.42	8.70	5.98		2.47
LUT 1	FLOW	660. CFS	F	AN DRAG	4200. LB-	
DRIVER ACC	-0.010	22	9.67	0.84		1.17
G,#1	0.299	1.00	-0.64	-0.79		-0.90
TROOF ACC	0.008	27	0.63	0.81		1.24
G,#1	0.320	<b>0.9</b> 0	-0.58	-0.74		-1.00
HOR ACC G:#1	-0.128 0.187	56 0.25.	0.14	0.27 -0.57		0.53 -0.87
CUSH PRESS	68.313	16	91.43	95.89		98.91
PSF	7.466	32.00	49.04	.43.92		38.01
TRUNK PRESS	116.676	57	161.08	178.79	200.04	258.64
PSF	19.096	48.00	86.01	73.76	63.58	58.19
LVT 2	FLOW	630. CFS	F	AN DRAG	4070. LB-	
DRIVER ACC	0.011	42	0.62	0.86		1.08
G,#2	0.306	0.60	-0.50	-0.70		-0.82
TROOF ACC G,#2	0.000 0.256	41 0.50	0.48	0.64 -0.59		0.95 -0.78
HOR ACC	-0.045	54	0.21	0.34	0.43	0.46
G∙≢2	0.140	0.25	-0.26	-0.37	-0.45	-0.52
CUSH PRESS	75.864		95.84	104.01	111.97	124.70
PSF	11.819		56.61	49.84	46.30	44.12
TRUNK PRESS PSF	119.228 9.500		147.79 94.13			166.60 78.30

			TR	-2299		
	DAVIDSON LABORATORY		TAB	LE 9-3		· F
DAVIDSON			ACV BARGE TRAIN			22-9
			(Con	tinued)		
RUN 125						
	SPEED	12.5	MEH		i	WAVE ENCOUNTER
	WEIGHT	30000.			`	SEA STA
-	DRAG	14180.	LB			LCG 110
	4	IEAN/RMS	OSC/BUFF	AVG	1/3	1/10 EX
LVT 3		FLOW	650. CF9	SFAI	N DRAG	4300. LB
DRIVER AC			34			
G,#3				0.52 -0.50	-0.70	-
TROOP ACC		-0.002	41	0.42	0.60	
G•#3		0.242	0.45	-0.40	-0.54	
HOR ACC			40	0.42	0.60	
G•#3		0.155	0.35	-0.21	-0.34	-
CUSH FRES	S	74.153	39	92.26	99.24	10
PSF		10.676	24.00	53.34	42.76	<del>-</del> 1
TRUNK PRE	SS	121.087		143.29		15
F'SF		9.855	36.00	96.83		8
LUT 4		FLOW	640. CFS	FAI	N DRAG	4100. LB
DRIVER AC	С	-0.019	5	0.25		
G, #4		0.148	0.60	-0.66		-
TROOP ACC		-0.056	42	0.41	0.61	
G + #4		0.244	0.50	-0.42	-0.56	
HOR ACC G:#4		0.100 0.134	21	0.46	0.62	

72.447 35

10.746 24.00

14.159 36.00

45

117.676

91.29

53.20

145.05

92.06

99.12

44.15

154.00

83.47

111.34

29.32

163.24

73.83

CUSH PRESS

TRUNK PRESS

F'SF

FSF

FAGE 1

DAVIDSON LABORATORY

#### TABLE 9-4 ACV BARGE TRAIN

22-SEF-82

#### FOUR UNITS, LCAC TOW, 13.3 FT SPACING, TRACKS DOWN

	WEIGHT	15.0 30000. 12410.	LB				NTERS 38 STATE 2 110.0 IN
	М	EAN/RMS	OSC/BUFF	AVG	1/3	1/10	EXTREME
DRAG TFS		12.415 3.561	39 3.42				22.92 3.46
LUT 1	\ <b>-</b>	FLOW	660. CFS	F	AN DRAG	3410. LB-	
DRIVER AC	cc		30 1.00				2.05 -1.06
TROOF ACC		-0.011 0.385					1.60 -1.02
HOR ACC G•#1						0.41 -0.68	
CUSH PRES						132.92 12.73	
TRUNK PRE						227.35 49.19	
L.VT 2	?	FLOW	620. CFS	;	AN DRAG	3360. LB-	~~~~~
DRIVER AC	cc	0.011 0.364	43 0.60				1.49 -1.01
TROOF ACC	2	0.003	38 0.50				0.81 -0.99
HOR ACC G,#2			70 0.25			0.64	
CUSH FRES	68	78.084 13.463		99.02 54.83	109,69 41.35		119.90 -1.60
TRUNK FRE PSF	ESS	120.050 16.979	36 40.00	151.63 89.87			169.10 69.97

PAGE 2

DAVIDSON LABORATORY

## TABLE 9-4 ACV BARGE TRAIN (Continued)

22-SEF-82

<b>C</b> 1	HN	4	26	,
TC.	UIN			٠,

WEI	ED 15.0 GHT 30000. G 12410.	LB		I		STATE 2 110.0 IN
-	MEAN/RMS	OSC/BUFF	AVG	1/3	1/10	EXTREME
LVT 3	FLOW	640. CFS	;F	AN DRAG	3610. LB	
DRIVER ACC G:#3	0.016 0.395					1.19 -1.00
TROOP ACC G+#3	-0.007 0.292	43 0.45	0.50 -0.42	0.71 -0.61		1.00 -0.79
HOR ACC G•#3					0.78 -0.66	
CUSH PRESS PSF	70.765 14.145			103.99 29.93		117.61 4.81
TRUNK PRESS PSF	119.626 14.258					163.16 69.17
LUT 4	FLOW	680. CF9	F	AN DRAG	3610. LB	
DRIVER ACC G:#4	-0.126 0.328	21 0.60	0.35 -0.76	0.52 -1.13		0.58 -1.35
TROOP ACC G,#4	•	33 0.50				0.76 -1.00
HOR ACC G+#4	0.081 0.154	25 0.40				0.79 -0.32
CUSH FRESS FSF	66.950 11.543	22 24.00	86.33 44.36	94.85 28.23		108.96 6.34
TRUNK PRESS PSF	117.550 15.974	36.00	1 <b>46.64</b> 90.00	159.06 77.17		172.02 64.41

DAVIDSON LABORATORY

### TABLE 9-5

### 28-0CT-82

### ACV BARGE TRAIN

### FOUR UNITS, LCAC TOW, 13.3 FT SPACING, TRACKS DOWN

RUN 128 , 127

	WEIGHT	20.0 30000. 12790.	LB				NTERS 43 STATE 2 110.0 IN
		MEAN/RMS	OSC/BUFF	AVG	1/3	1/10	EXTREME
DRAG KIFS		12.792 2.877	43 3.42	16.55 8.62	19.02 6.50	1	21.38 4.72
LVT	1	FLOW	CFS	F	AN DRAG	LF-	
DRIVER A G,#1	CC	-0.009 0.597	46 1.00				3.47 -1.18
TROOF AC G•#1	С					1.36 -0.85	
HOR ACC G##1		-0.085 0.207	71 0.25	0.23 -0.36	0.44 -0.50	0.58 -0.63	0.75 -0.80
CUSH PRE PSF	SS	75.497 27.382	86 32.00	121.38 44.36	150.33 25.94	180.51 12.10	208.88 4.06
TRUNK FR PSF	ESS	39.424					
LVT	2	FLOW	630. CFS	F	AN DRAG	2430. LP-	
DRIVER A G•#2	CC					2.04 -1.09	
TROOF AC	С	0.002 0.324	61 0.50	0.57 -0.41	0.82 -0.62	0.98 -0.76	1.26 -1.00
HOR ACC G+#2	•	-0. <b>05</b> 1 0.170	74 0.25	0.22 -0.31	0.39 -0.45	0.59 -0.55	0.87 -0.67
CUSH PRE PSF	SS	68.258 26.972	66 2 <b>4.</b> 00	116.57 38.68	158.10 17.40		235.65 -10.23
TRUNK FR	ESS	112.537 22.161	50 40.00	153.07 81.20	171.50 68.79		195.75 49.15

PAGE 2

28-0CT-82

TABLE 9-5 DAVIDSON LABORATORY ACV BARGE TRAIN

(Continued)

NUR IZO , IZ(	KUN	128,	127
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KOK II.	1 . TE						
	SPEED WEIGHT DRAG	20.0 30000. 12790.	MPH LB LB				NTERS 43 STATE 2 110.0 IN
		MEAN/RMS	OSC/BUF	F AVG	1/3	1/10	EXTREME
LUT	3	FI (16)	AAO. CE	'SE	AN TIPAC	2700. LB-	
DRIVER A	ACC	0.016	49	0.65	0.95		1.58
G•#3		0.401	0.60	-0.50	-0.74		-0.86
TROOP A	CC	-0.004	46	0.48	0.49		1.02
G•#3		0.275	0.45	-0.41	-0.54		-0.77
HUE VCC							
G + #3		0.044 0.187	4/	0.37	0.53		0.92
<b>374</b> 3		0.18/	0.35	-0.28	-0.47		-1.06
CUSH PRE	ESS	70.481	53	99.46	118.35	144.43	224.50
FSF		16.619	24.00	46.18	25.05	3.82	-27.37
TOTAL DE							
PSF	(E35	119.380	46	151.36	162.45		182.71
, 0.		18.811	30.00	92,02	80.36		56.39
LVT	4	FLOW	630. CF	8F	AN DRAG	2520. LB-	
DRIVER 4	20C	-0.068	1.0	A =A	0 70		
G,#4	.00	0.209	0.60	0.50	0.70		1.00
TROOP AC	CC	-0.035	45	0.48	0.73		1.06
G,#4		-0.035 0.266	0.50	-0.40	-0.40		-0.85
HOR ACC		0.059	24	0.44	0 70		
G , #4		0.059 0.162	0.40	-0.21	-0.34		1.18
							-0.49
CUSH FRE	SS	72.303	42	98.28	109.67		121.25
PSF		18.631	24.00	45.13	25.39		5.55
TRUNK PR	FSS	114 017	40	157 54			
FSF		116.813	47 34.00	153.94	1/4.00		222.29
. <b>-</b> .		20.359	30.00	07.72	/6+28		63.62

DAVIDSON LABORATORY

### TABLE 9-6

28-0CT-82

### ACV BARGE TRAIN

FOUR UNITS, LCAC TOW, 13.3 FT SPACING, TRACKS DOWN

RUN 137 , 136

	•						
	WEIGHT	25.0 30000. 13300.	LB				NTERS 37 STATE 2 110.0 IN
	М	EAN/RMS	OSC/BUFF	F AVG	1/3	1/10	EXTREME
DRAG KIPS		13,298 3,427	34 3.42	18.30 8.74	21.98 6.77		28.50 4.17
LVT 1		FLOW	700. CFS	6F	AN DRAG	2320. LB-	
DRIVER AC G,#1	C	0.006 0.7 <b>48</b>	54 1.00	1.61 -0.74	2.34 -1.10	2.82 -1.25	3.14 -1.39
TROOF ACC G,#1							
HOR ACC G,#1		-0.073 0.228	63 0.25	0.27 -0.36	0:47 -0 <b>:</b> 54	0.62 -0.73	0.77 -0.87
CUSH FRES PSF	S	67.883 36.304	76 32.00	128.47 30.67	158.75 6.83	180.98 -4.11	
TRUNK FRE	SS	121.810 43.883	76 <b>48.0</b> 0	205.27 79.00	253.32 59.34	294.71 47.28	321.68 29.10
LUT 2		FLOW	670, CFS	F	AN DRAG	2070. LB	
DRIVER ACC G,#2	C	0.014 0.583	53 0.60	1.00	1.49 -0.98	1.83 -1.11	2.09 -1.23
TROOF ACC G,#2		0.002 0.438	52 0.50	0.73 -0.47	1.00 -0.79	1.14 -0.95	1.33 -1.03
HOR ACC G,#2		-0.054 0.197	63 0.25	0.21 -0.35	0.39 -0.52	0.52 -0.70	
CUSH PRESS PSF	6	63.109 30.007	66 24.00	106.91 30.09	132.17 11.54	149.09 1.23	161.47 -15.35
TRUNK PRES	SS :	112.996 26.575		157.31 79.94	176,27 65,57	184.78 58.45	191.59 50.81

DAVIDSON LABORATORY

### TABLE 9-6

### 28-0CT-82

### ACV BARGE TRAIN (Continued)

RUN 137 , 136

	SPEED WEIGHT DRAG	25.0 30000. 13300.	MPH LB LB			SE	DUNTERS 37 EA STATE 2 CG 110.0 IN
		MEAN/RMS	OSC/B	UFF AV	3 1/3		) EXTREME
LVT	3	FLOW	730.	CFS	FAN DRAG	2400. LI	3
	CC	0.017	46	0.8	36 1.2	4	1.73
0,43		0.485	0.60	-0.5	50 -0.7	9	-0.94
TROOP ACC	3	0.000 0.344	45 0.45	0.5	59 0.9: 14 -0.6	1	1.45 -0.79
							-0.79
HOR ACC S,#3		0.033	45	0.3	39 0.6. 29 -0.45	3	1.15
3,43		0.206	0.35	-0.2	29 -0.45	5	-0.73
CUSH PRES	S	60.594	52	91.4	2 113.30	177 (/	170 04
FSF		27.419	24.00	25.3	6 -3.18	3 -23.12	132.04
TRUNK 665							3/•3/
PSF	255	120.151	48	162.8	88 179.18	3	187.22
rar		20.833	36.00	87.8	69.83	3	54.14
LVT 4							
DRIVER AC	22	0.011	46	0.8	1.19	?	1.98
G <b>, #</b> 4		0.461	0.60	-0.5	1.19 3 -0.78	5	-0.92
G > #4	,	0.320	0.50	-0.5	7 0.90 2 -0.40	)	1.19
							-0.82
HOR ACC		0.055	24	0 • 4	5 0.61		0.84
G•#4		0.180	0.40	-0.2	4 -0.35	5	-0.44
CUSH PRES	S	44 441	40	07.4			
PSF		22.264	74.00	7/•1	4 111.99 3 19.34	,	131.15
							-3.17
TRUNK FRE	SS	115.558	53	160.3	1 183.19	204.61	221.50
PSF		26.341	36.00	83.1	1 70.39	61.27	51.06

PAGE 1

28-OCT-82

TABLE 9-7

ACV BARGE TRAIN

FOUR UNITS, LCAC TOW, 13.3 FT SPACING, TRACKS DOWN

RUN 131 , 129

DAVIDSON LABORATORY

		30.0 30000				WAVE ENCOU	NTERS 32 STATE 2
		14550.					110.0 IN
		MEAN/RMS	OSC/BUFF	AVG	1/3	1/10	EXTREME
DRAG		14,546					31.96
KIPS		5.330	3.42	8.29	5.59		1.01
LVT 1	1	FLOW	680. CFS	F	AN DRAG	1790. LB-	
DRIVER AC	30	-0.001	49 1.00	1.54	2.28	}	3.56
G•#1		0.770	1.00	-0.68	-1.06	•	-1.37
TROOP ACC	2	0.014	46	1.04	1.38	1	1.98
G,#1		0.556	0.90	-0.63	-0.93	}	-1.17
HOR ACC		-0.060	56	0.28	0.46	0.63	0.81
G•#1		0.253	0.25	-0.38	-0.58	-0.66	-0.79
CUSH FRES	SS	62,989	60	127.85	155.70	175.92	210.36
FSF		36.932	32.00	24.92	2.51	-3.81	-9.60
TRUNK FRI	ESS	114.944	66	207.01	260.40	297.78	359.67
PSF		47.472	48.00	72.42	45.26	30.25	19.40
LVT	2	FLOW	560. CF9	3F	FAN DRAG	1340. LB-	
DRIVER A	cc	0.005	47	1.09	1.72	2	2.91
G•#2		0.647	0.60	-0.61	-1.01	Ĺ	-1.20
TROOF AC	С	-0.013	46	0.85	1.29		2.05
G•#2		0.524	0.50	-0.58	-1.01	Į.	-1.39
HOR ACC		-0.023	54	0.31	0.51	0.61	0.67
G • #2		0.243	0.25	-0.37	-0.55	-0.68	-0.75
CUSH PRE	SS	71.455	60	121.29			
PSF		33.452	24.00	40.07	21.0	5 7.67	-15.35
TRUNK PR	ESS	106.016	46	154.46	1.75.50		196.58
PSF		29.630	40.00	71.13	52.74	4	28.32

TABLE 9-7
ACV BARGE TRAIN
(Continued)

PAGE 2

28-0CT-82

DAVIDSON LABORATORY

RUN 131, 129

WEIG	TD 30.0 GHT 30000. G 14550.	LB				NTERS 32 STATE 2 110.0 IN
	MEAN/RMS	OSC/BU	FF AUG	1/3	1/10	EXTREME
LVT 3	FLOW	710. C	FSF1	AN IIRAG	1890. LB-	
DRIVER ACC	0.010	45	1.06	1.66		2.37
G,‡3	0.605	0.60	-0.61	-0.99		-1.15
TROOF ACC	-0.007	53	0.64	0.97	1.13	1.19
G• <b>*</b> 3	0.397	0.45	-0.44	-0.73	1.13 -0.90	-1.15
HOR ACC	0.007	45	0.41	0.64		0.94
G• ‡3	0.257	0.35	-0.39	-0.54		-1.23
CUSH PRESS	59.943	61	97.99	122.62	140,97	163.48
PSF	30.793	24.00	23.04	1.34	-11.41	-33.66
TRUNK PRESS	116.347	48	164.41	188.25		223.31
PSF	30.178	36.00	81.95	60.39		44.36
LVT 4	FLOW	570. CF	'SFA	N DRAG	1500. LB-	
DRIVER ACC	0.150	54	0.93	1.31	1.56 -0.89	1.85
G • #4	0.581	0.40	-0.48	-0.76	-0.89	-0.96
TROOF ACC		23	0.56	0.81		0.96
G, #4	0.249	0.50	-0.40	0.57		-0.77
HOR ACC	0.044	24	0.56	0.85		1.27
G, ‡4	0.234	0.40	-0.29	-0.41		-0.63
CUSH FRESS	79.398	45	112.62	129.01		137.89
PSF	22.022	24.00	53.95	33.36		14.26
TRUNK PRESS	115.717	47	170.51	200.83		248.99
F'SF	115.717 31.062	36.00	81.67	65.54		33.78

TABLE 9-8

DAVIDSON LABORATORY A

### ACV BARGE TRAIN

28-0CT-82

FOUR UNITS, LCAC TOW, 13.3 FT SPACING, TRACKS DOWN

RUN	135 .	134

, , _ , , , , , , , , , , , , , , , , ,	, -5						
	WEIGHT	35.0 30000. 16470.	LB		ı		NTERS 33 STATE 2 110.0 IN
				AVG	1/3	1/10	EXTREME
DRAG KIPS		16.47 <b>4</b> 5.683	24 3.42	23.53 9.59	29.6 <b>5</b> 6.70		32.57 3.84
LVT	1	FLOW	528. CF9	6F <i>F</i>	AN DRAG	1104. LB-	
DRIVER AU G:#1	CC	-0.006 0.844	39 1.00				3.90 -1.42
TROOF ACC		-0.006 0.548	23 0.90	1.12 -0.59	1.45 -0.85		1.57 -1.17
HOR ACC		-0.048 0.307				0.98 -0.79	
CUSH PRES	SS	76.421 36.828	59 32.00	138.43 40.46	174.19 15.63	194.37 6.83	207.78 -2.58
TRUNK PRI PSF	ESS	107.318 53.431	33 48.00	197.92 58.88	262.39 34.53	) 3	345.12 -4.04
LVT	5	FLOW	640. CFS	5F	AN IIRAG	1370. LB-	
DRIVER A		0.012 0.660	42 0+60				4.14 -1.17
TROOF AC	С	-0.003 0.485	40 0.50	0.91 -0.50	1.37 -0.84		2.70 -1.24
HDR ACC G•#2			51 0.25	0.35	0.60 -0.61	0.77 -0.80	
CUSH PRE PSF	SS	65.135 33.909	52 24.00	118.28 33.94	161.26 5.77		
TRUNK PR	ESS	110.154 30.233	41 40.00	162.55 73.57	187.84 59.20		219.91 41.65

PAGE 2

DAVIDSON LABORATORY

## TABLE 9-8 ACV BARGE TRAIN (Continued)

28-0CT-82

RUN 135 , 13	4					
WEIG	II 35.0 HT 30000. 16470.	LB				NTERS 33 STATE 2 110.0 IN
	MEAN/RMS	OSC/BUF	F AVG	1/3	1/10	EXTREME
LUT 3	FLOW	690. CF		AN DRAG	1590. LB-	
DRIVER ACC	0.004	45	1.02	1.61		2.36
	0.604					
TROOP ACC	-0.007	<b>1</b>	0.49	1 04		1.51
G+#3	0.397					-1.03
HOR ACC	0.048	42	0.48	0.79	0.94	1.17
G•#3	0.278	0.35	-0.36	-0.62	-0.83	-1.13
CUSH FRESS	65.187	49	107.66	127,56		156.45
PSF	32.970	24.00	24.52	-0.63		-14.79
TOUR DEFEN	440.000		<del></del>			
TRUNK PRESS FSF	118+209	50 77 AA	163.41	186.69	199.40 54.59	212.78
ror	20+343	30.00	84.76	6/,78	34,37	45.11
LUT 4	FLOW	610. CF	SF	AN DRAG	1340. LB	
DRIVER ACC	0.013 0.655	41	1.15	1.69		2.73
G+#4	0.655	0.40	-0.60	-1.05		-1.27
TROOF ACC	-0.021	39	0.81	1,20		1.65
G•#4	-0.021 0.497	0.50	-0.54	~0.87		-1.11
HOR ACC	0.027	27	¢ (5	() () <del>""</del>		
Gy#4	0.798	دن ۱.۵۵	0.62 -0.40	U+B/ () 41		1.22
<b>₩</b> 7.83	V•2/0	V• 7V	-0.40	-0.81		-0.96
CUSH FRESS	72.754	44	112.36	138.37		201.29
F'SF	27.685	24.00	41.26	22.93		10.70
TRUNK PRESS	117 404	E* 1	1 ~7 ~7 4 4	73.0 79 . 77 4	A M	
TRUNK PRESS PSF	37.130	74 VV	79.15	203.76	227.13	
,	□/ + I ∪ U	20+00	ノグ・エコ	55.95	43.72	35.35

BAVIDSON LABORATORY

### TABLE 9-9

#### - <del>-</del>

28-00T-82

### ACV BARGE TRAIN

FOUR UNITS, LCAC TOW, 13.3 FT SPACING, TRACKS DOWN

RUN 133 , 132

190日間ではあるの間であるのである。 190日には、19日には、190日には、1

SFEED 44.8 MFH WEIGHT 30000. LB DRAG LB

WAVE ENCOUNTERS 28 SEA STATE 2

LCG 110.0 IN

MEAN/RMS OSC/BUFF AVG 1/3

/3 1/10 EXTREME

	FLOW	620. C	FSF	AN DRAG	1090. LB
DRIVER ACC	0.013	33	2.22	3.23	4.81
G,#1	1.035	1.00		-1.30	-1.64
TROOP ACC	0.066	33	i.32	1.93	2.70
G • #1			-0.56		-1.01
HDR ACC	-0.038	41	0.36	0 (1	
G v #1	0.266		-0.39		0.82 -0.82
CUSH FRESS	77. 450	ΛE	151.45	204.07	
PSF	47.516			-6.13	264.98 -47:98
TRUNK PRESS	115.794	40	220 (4	714 04	
FSF	65.971		59.64		452.62 -3.23
LVT 2	FLOW	586. C	FSF <i>F</i>	AN IIRAG	951. LB
	0.022	34		2.88	951. LB 3.82 -1.33
DRIVER ACC	0.022 0.863	34 0.60	1.75 -0.71	2.88 -1.11	3.82 -1.33
DRIVER ACC G,#2	0.022 0.863 0.006	34 0.60 36	i.75	2.88 -1.11	3.82
DRIVER ACC Gy#2 TROOF ACC	0.022 0.863 0.006 0.519	34 0.60 36 0.50	1.75 -0.71 1.02 -0.52	2.88 -1.11 1.76 -0.78	3.82 -1.33 3.00 -0.98
DRIVER ACC Gy#2 TROOP ACC Gy#2	0.022 0.863 0.006 0.519	34 0.60 36 0.50	1.75 -0.71 1.02 -0.52	2.88 -1.11 1.76 -0.78	3.82 -1.33 3.00
DRIVER ACC Gy#2 TROOP ACC Gy#2 HOR ACC	0.022 0.863 0.006 0.519 -0.018 0.261 68.658	34 0.60 36 0.50 44 0.25 24	1.75 -0.71 1.02 -0.52 0.33 -0.37	2.88 -1.11 1.76 -0.78 0.55 -0.55	3.82 -1.33 3.00 -0.98 0.86 -0.90
DRIVER ACC G,#2 TROOP ACC G,#2 HOR ACC G,#2	0.022 0.863 0.006 0.519 -0.018 0.261	34 0.60 36 0.50 44 0.25 24	1.75 -0.71 1.02 -0.52 0.33 -0.37	2.88 -1.11 1.76 -0.78 0.55 -0.55	3.82 -1.33 3.00 -0.98
DRIVER ACC G, #2 TROOP ACC G, #2 HOR ACC G, #2 CUSH PRESS FSF	0.022 0.863 0.006 0.519 -0.018 0.261 68.658	34 0.60 36 0.50 44 0.25 24 24.00	1.75 -0.71 1.02 -0.52 0.33 -0.37 135.26 38.40	2.88 -1.11 1.76 -0.78 0.55 -0.55 195.04 9.87	3.82 -1.33 3.00 -0.98 0.86 -0.90 287.13

DAVIDSON LABORATORY

TABLE 9-9

28-0CT-82

## ACV BARGE TRAIN (Continued)

RUN	133		132
NUN	100	•	1)2

	D 44.8 HT 30000.				WAVE ENCOUNTERS 28 SEA STATE 2 LCG 110.0 IN
	MEAN/RMS	OSC/BU	F AVG	1/3	1/10 EXTREME
LVT 3	FLOW	65 C	FSF	AN DRAG	1140. LB
DRIVER ACC	0.021	<b>3</b> 9	1.05	1.66	3.07
G,#3	0.598	0.60	-0.59	-0.92	-1.11
TROOF ACC	-0.)13	38	0.77	1.18	2.35
G:#3	0.450	0.45	-0.42	-0.69	-0.93
HUR ACC	0.025	29	0.42	0.62	0.79
G,#3	0.225	0.35	-0.33		-0.72
CUSH FRESS	67.001	37	108.29	129.22	144.98
FSF	34.533	24.00	24.47	-0.80	-21.82
TRUNK FRESS	114.363	43	161.76	185.61	213.53
FSF	32.453	36.00	77.20	57.09	41.35
LVT 4	FLOW	600. CF		N DRAG	1030. LB
DRIVER ACC	0.000	38	1.03	1.59	2.56
G, #4	0.652	0.60	-0.55	-1.01	-1.23
TROOF ACC	0.003	34	0.67	1.07	1.45
G,#4	0. <b>3</b> 97	0.50	-0.43		-0.78
HOR ACC	0.040	19	0.46	0.65	0.86
G•#4	0.210	0.40	-0.28	-0.45	-0.64
CUSH FIRESS	72.195	32	108.06	128.78	1.45 <b>.23</b>
PSF	27.226	24.00	40.84	19.60	7 <b>.9</b> 2
TRUNK PRESS	112.606	41	171.08	204.45	255 <b>.</b> 28
PSF	37.381	36.00	77.70	52.29	29 <b>.</b> 85

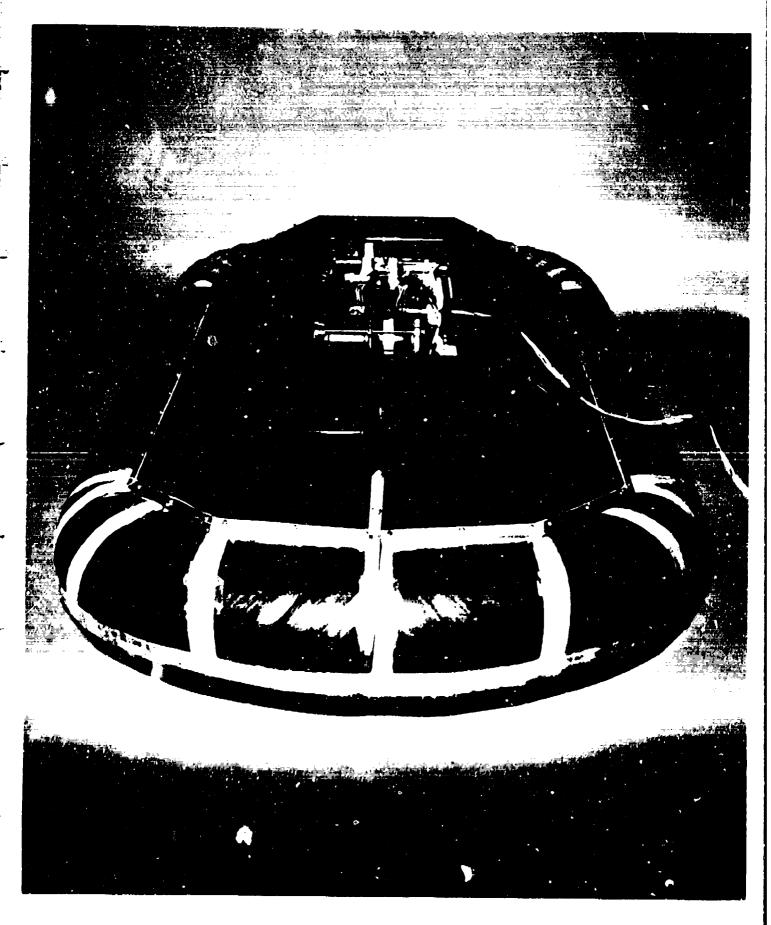
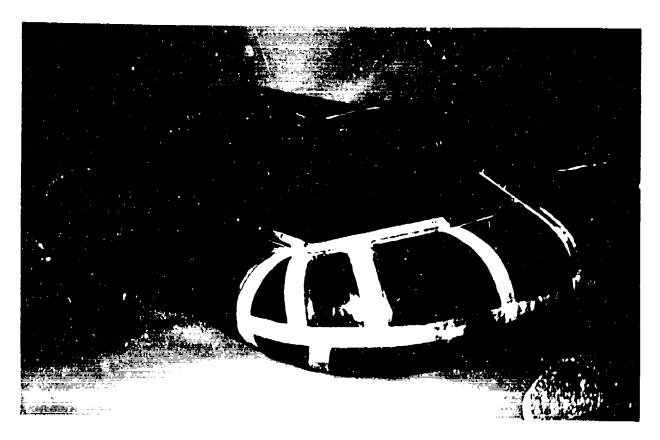
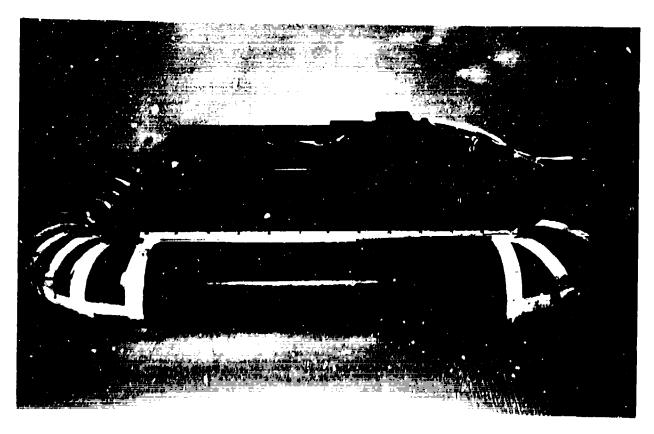


FIGURE 1 - BOW VIEW OF ACV MODEL ON CUSHION



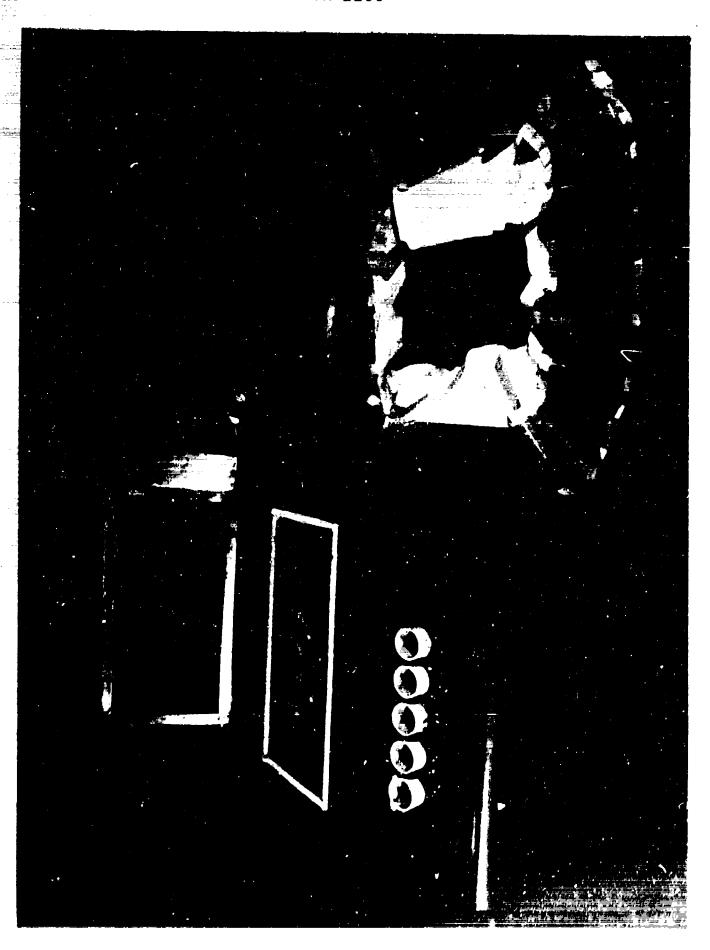
**BOW QUARTER VIEW** 

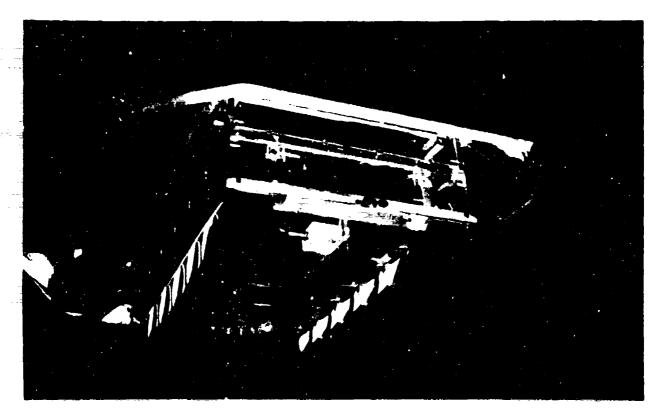


SIDE VIEW

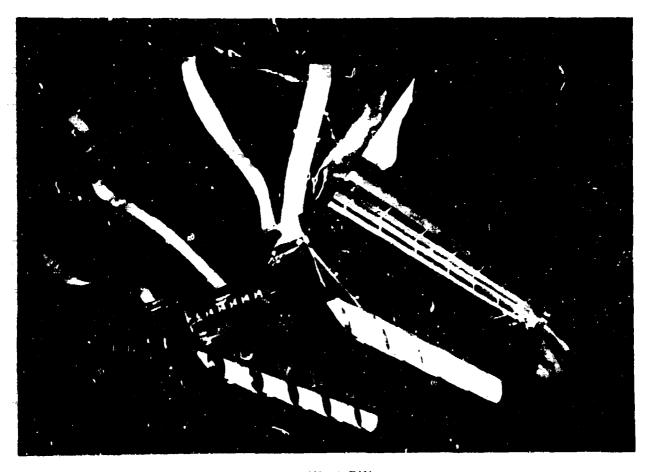
FIGURE 2 - ACV MODEL ON CUSHION







STERN VIEW



BOW VIEW

FIGURE & - UNDERSIDE OF ACV MODEL HULL



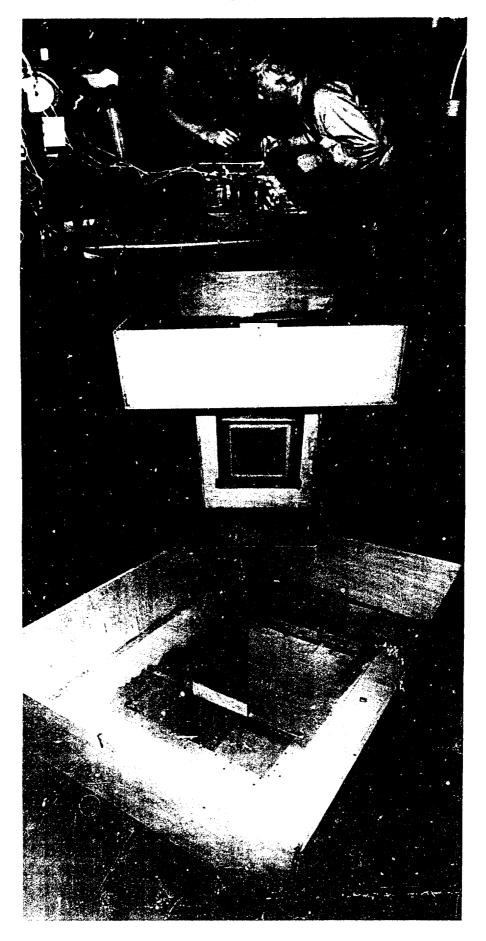
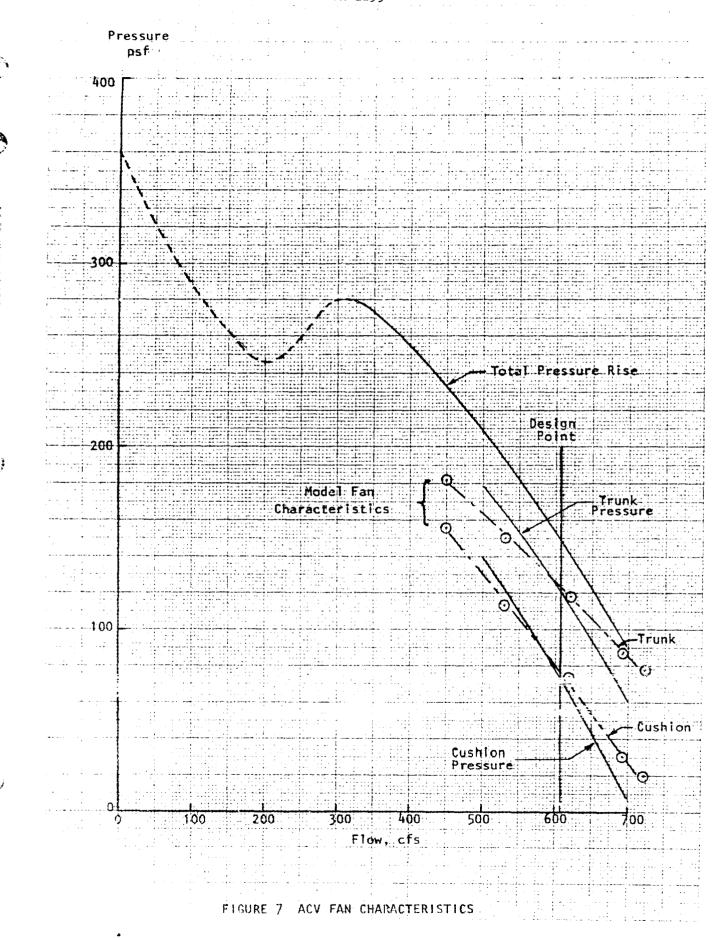
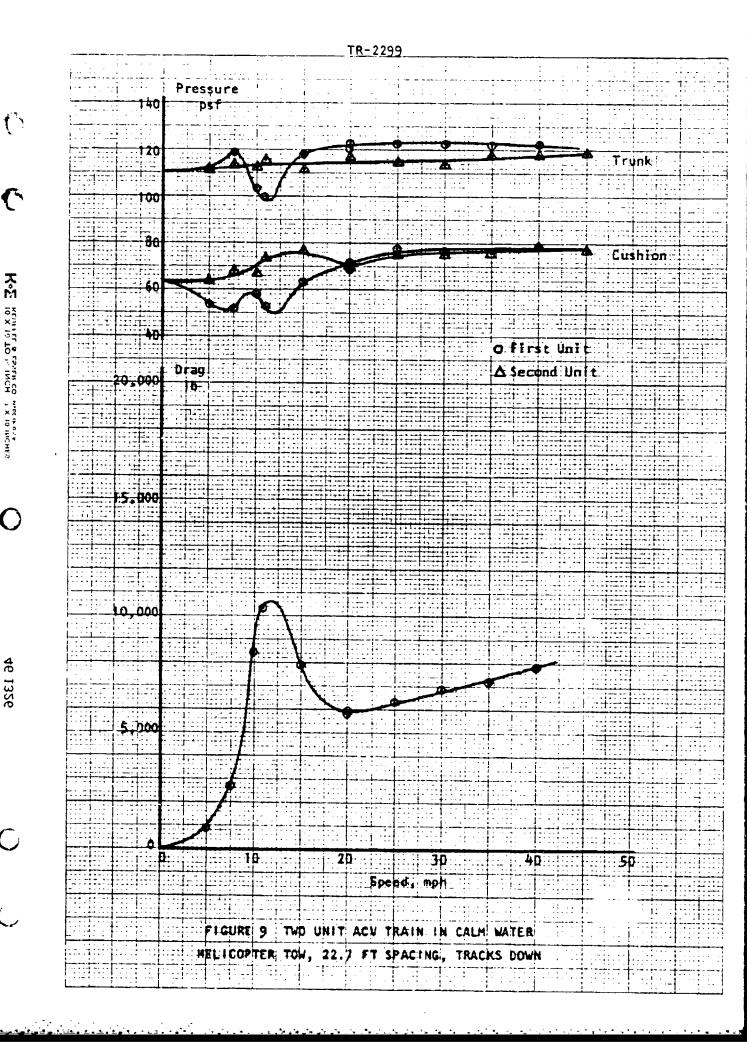


FIGURE A FAN CALIBRATION SETUP



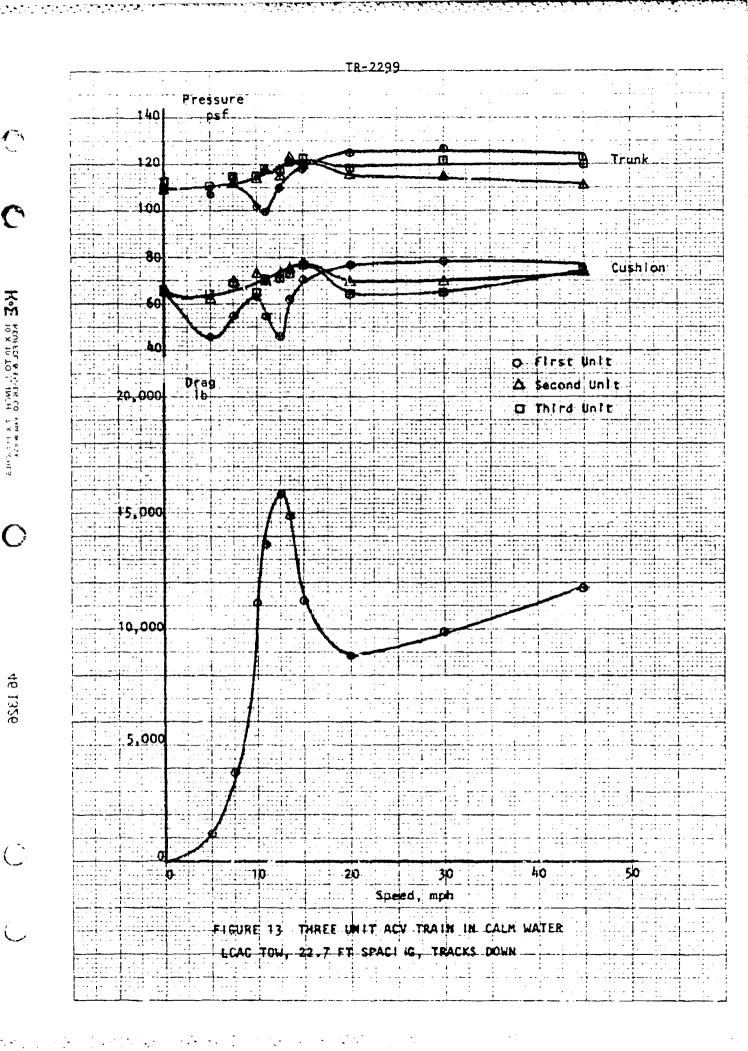
KEUFFEL & ESSER CO MACHINES

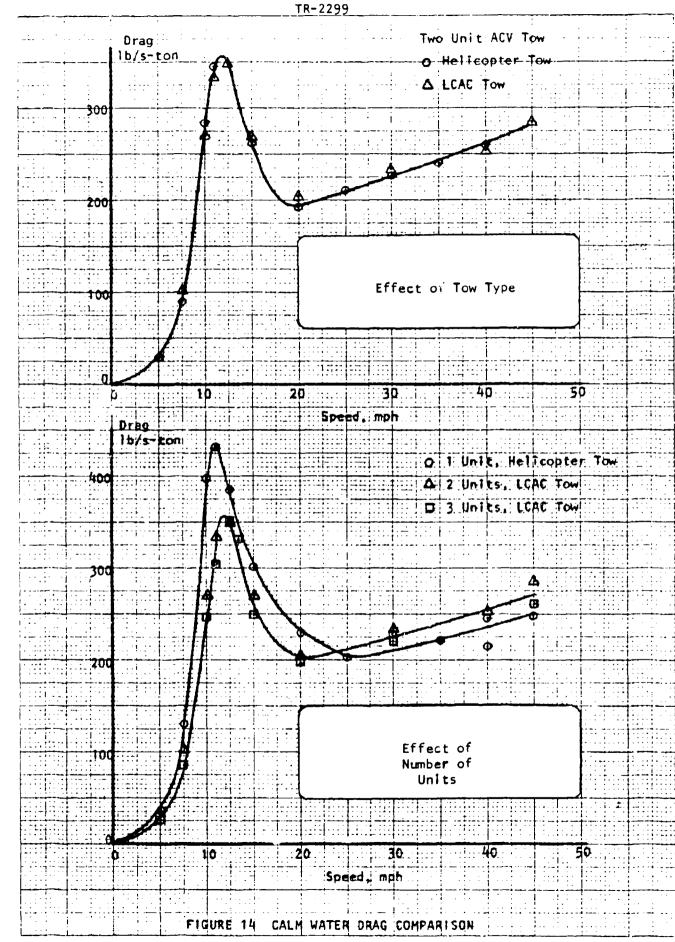


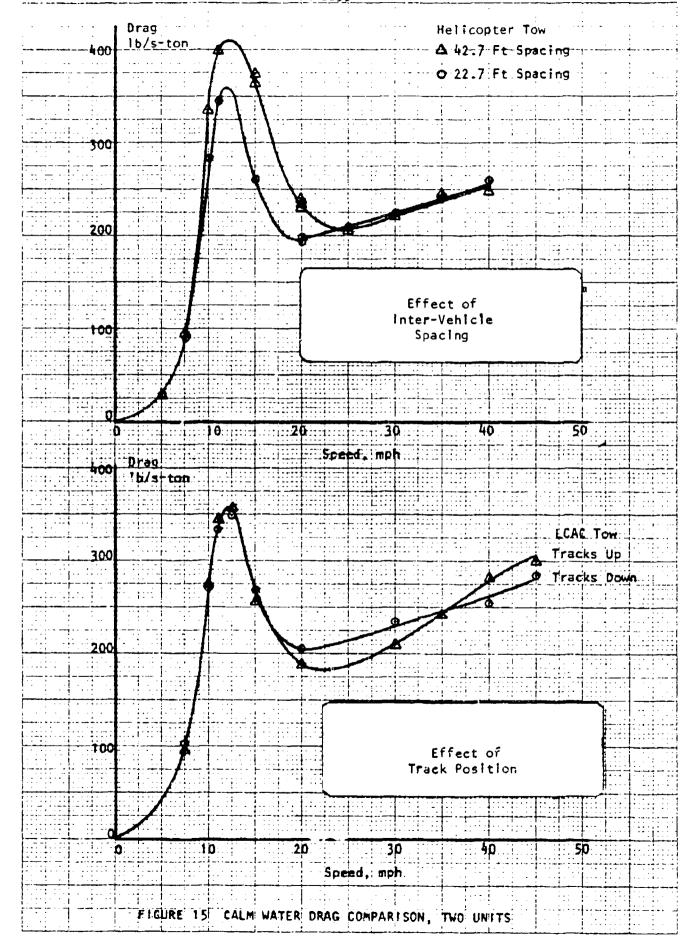
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ENCHANT OF THE MENT OF THE WASHINGTON

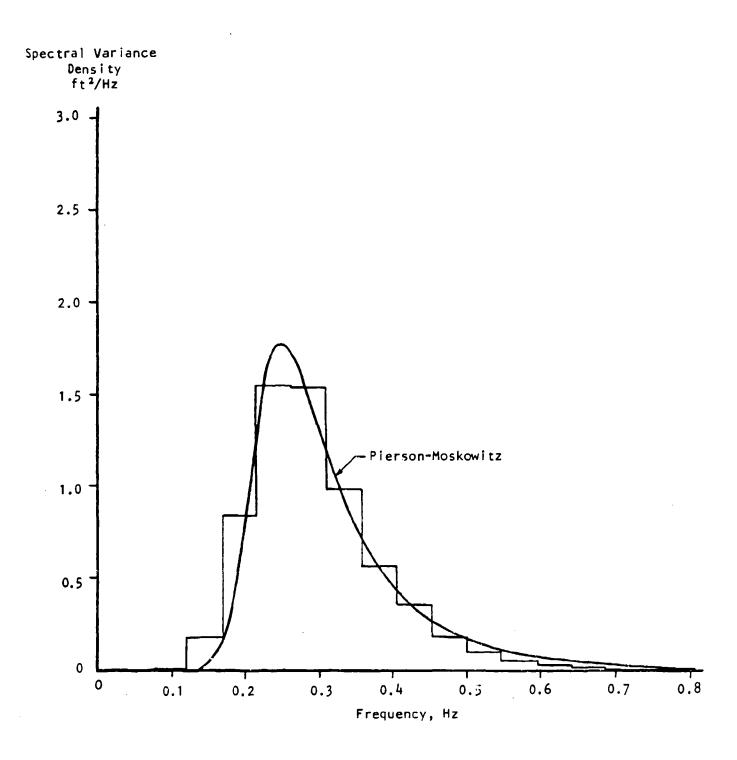
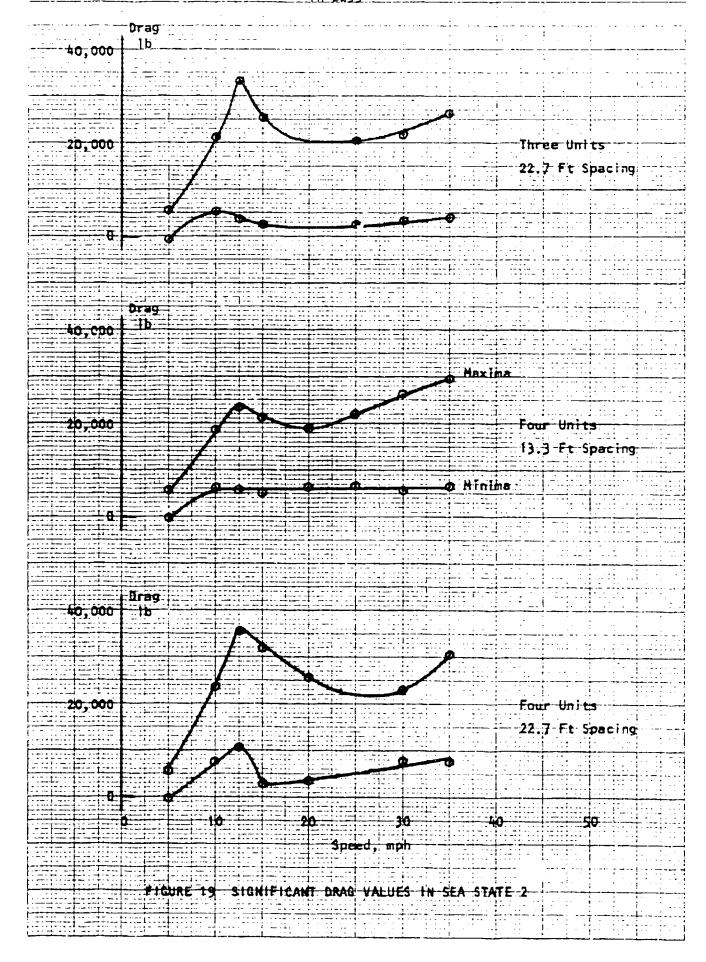
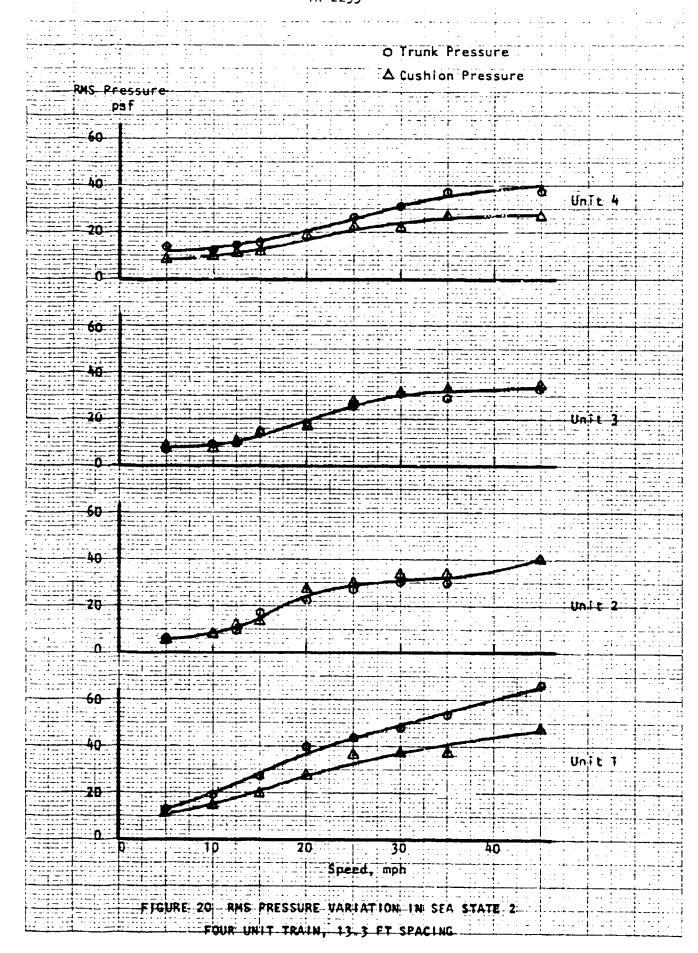


FIGURE 17 EXPERIMENTAL WAVE SPECTRUM SIGNIFICANT HEIGHT 2.2 FT

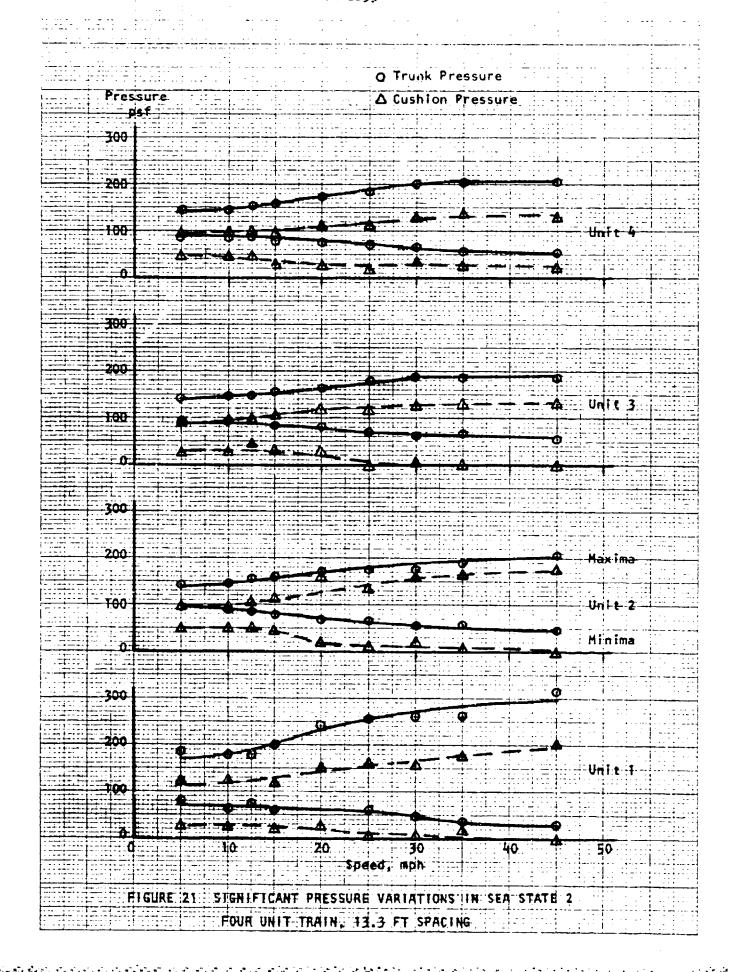


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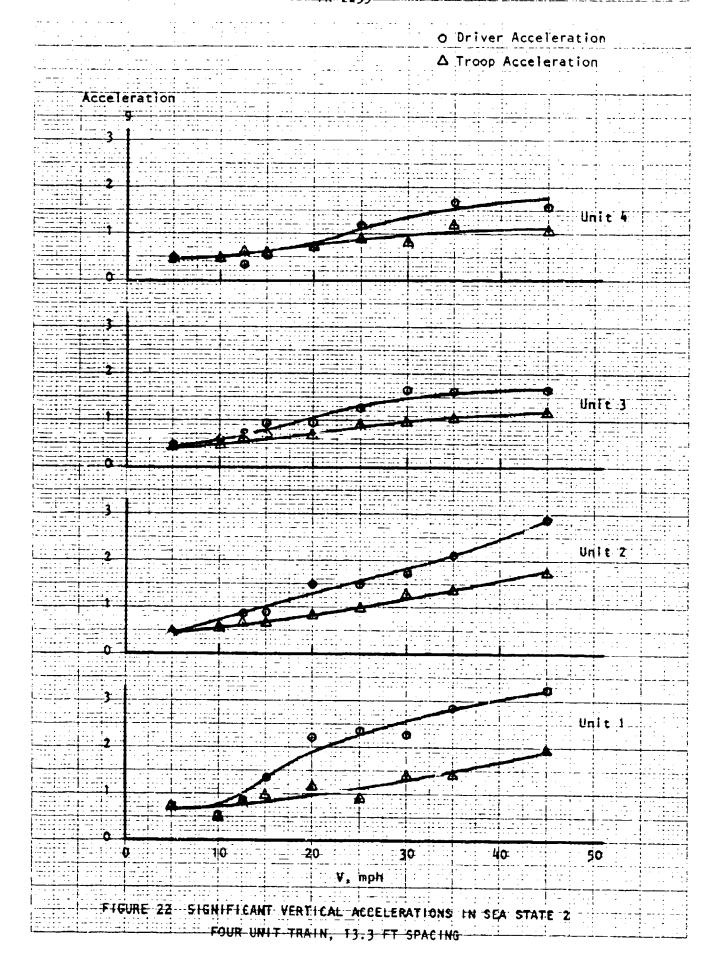
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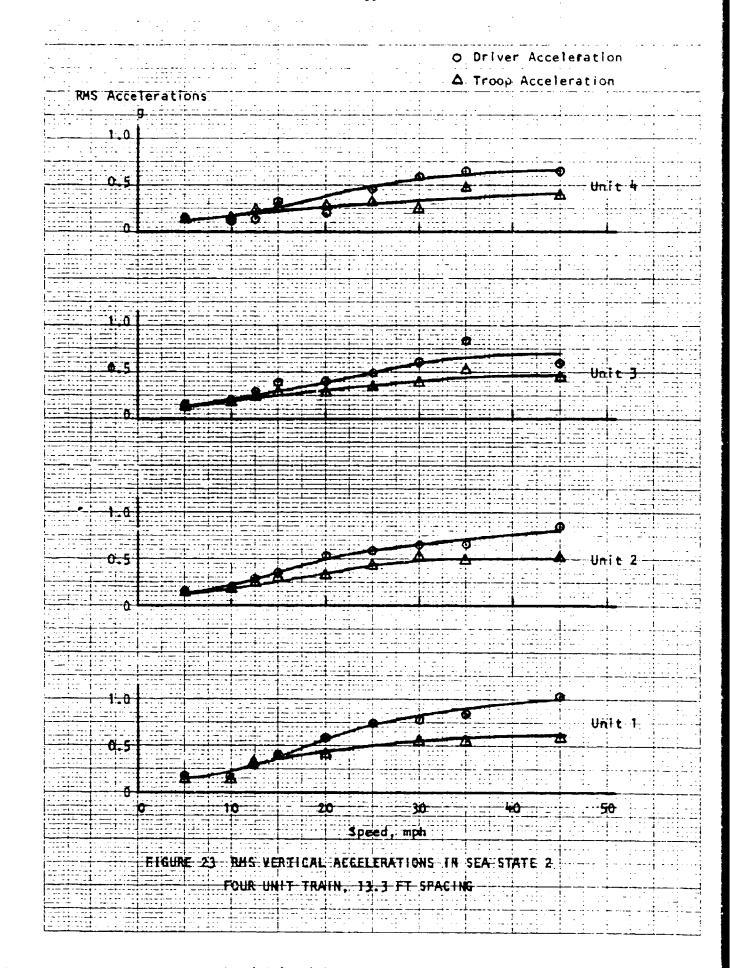


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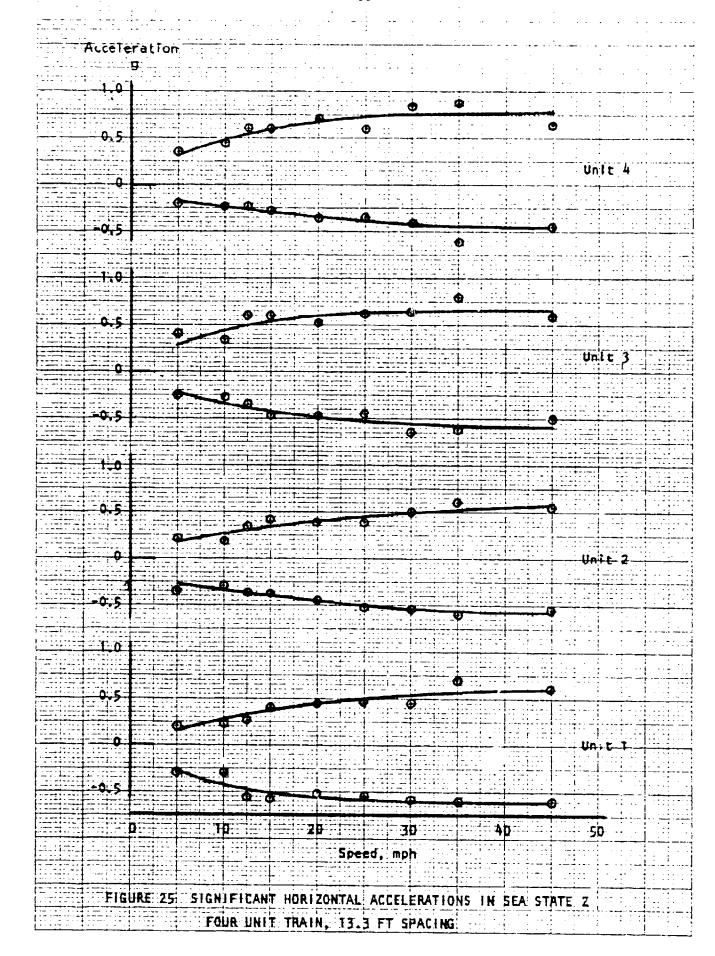


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APPENDIX
ACV BARGE TRAIN
VIDEO SCENARIO

SEA STATE	NO. OF UNITS	TYPE OF TOW	INTER- VEHICLE SPACING ft	TRACK CONFIGURATION	RUN	SHIP SPEED mph	FOOTAGE
Calm	1	Kelicopter	NA	Down	1	5.0	6
					2	5.0	14
					3	10.0	25
					4	15.0	30
					5	20.0	33
					6	25.0	35
					7	30.0	39
					8	35.0	43
					9	40.0	45
					10	40.0	46
					11	45.0	47
					12	7.5	48
					13	12.5	56
					14	11.0	60
				•	15	40.0	65
Calm	2	Helicopter	22.7	Down	16	5.0	69
					17	10.0	81
					13	10.0	86
					19	15.0	89
					20	15.0	94
					21	20.0	97
					22	20.0	103
					23	25.0	105
					74	30.0	107
					45	35.0	109
					26	40.0	111

# APPENDIX VIDEO SCENARIO (Continued)

SEA STATE	NO. OF UNITS	TYPE OF TOW	INTER- VEHICLE SPACING ft	TRACK CONFIGURATION	RUN	SHIP SPEED mph	FOOTAGE
Calm	2	Helicopter	22.7	Down	27	40.0	112
					28	45.0	113
					29	7.5	117
					30	7.5	120
					31	11.0	125
Calm	2	Helicopter	42.7	Down	32	5.0	128
					33	7.5	136
					34	10.0	141
					35	11.0	143
					36	15.0	148
					37	20.0	155
					38	25.0	160
					40	15.0	161
					41	20.0	164
					42	20.0	166
					43	25.0	169
					44	30.0	17.2
					45	35.0	175
					46	40.0	179
					47	45.0	180
Calm	2	LCAC	22.7	Down	49	7.5	182
					50	10.0	195
					51	11.0	197
					52	12.5	200
					53	15.0	204

APPENDIX
VIDEO SCENARIO
(Continued)

SEA STATE	NO. OF UNITS	TYPE OF TOW	INTER- VEHICLE SPACING ft	TRACK CONFIGURATION	RUN	SHIP SPEED mph	FOOTAGE
Calm	2	LCAC	22.7	Down	54	20.0	209
	_				55	30.0	212
					56	45.0	215
					57	40.0	217
Calm	3	LCAC	22.7	Down	59	5.0	219
					60	7.5	228
					61	10.0	233
					62	12.5	238
					64	15.0	241
					65	20.0	247
					66	30.0	249
					67	45.0	251
					69	11.0	252
					70	13.5	256
Calm	2	LCAC	22.7	Retracted	72	7.5	259
					73	10.0	265
					74	11.0	269
					75	12.5	273
					76	15.0	276
					77	20.0	279
					78	<b>30.</b> 0	281
					79	45.0	283
					80	40.0	288
					81	35.0	291

APPENDIX
VIDEO SCENARIO
(Continued)

SEA STATE	NO. OF UNITS	TYPE OF TOW	INTER- VEHICLE SPACING ft	TRACK CONFIGURATION	RUN	SHIP SPEED mph	FOOTAGE
2	3	LCAC	22.7	Down	86	5.0	304
-					87	10.0	312
					88	12.5	317
					89	15.0	320
					90	20.0	323
					92	30.0	325
					93	45.0	328
2	4	LCAC	22.7	Down	95	12.5	338
_					96	10.0	342
					98	10.0	348
					99	12.5	353
					100	15.0	356
					101	20.0	360
					102	30.0	363
					103	45.0	364
					105	25.0	367
					106	35.0	369
					107	45.0	371
					108	20.0	374
					109	30.0	377
					110	45.0	379
					111	35.0	381
2	3	LCAC	22.7	Down	112	10.0	383
-	-				113	12.5	389
					114	15.0	393

APPENDIX
VIDEO SCENARIO
(Continued)

SEA STATE	NO. OF UNITS	TYPE OF TOW	INTER- VEHICLE SPACING ft	TRACK CONFIGURATION	RUN	SHIP SPEED mph	FOOTAGE
2	3	LCAC	22.7	Down	115	20.0	397
					116	30.0	400
					117	25.0	402
					118	25.0	404
					119	35.0	406
					120	35.0	408
					121	45.0	409
	,		45.5	_	400	5.0	4.0
2	4	LCAC	13.3	Down	123	5.0	412
					124	10.0	417
					125	12.5	422
					126	15.0	426
					127	20.0	429
					128	20.0	432
					129	30.0	434
					130	30.0	438
					131	30.0	439
					132	45.0	441
					133	45.0	443
					134	35.0	444
					135	35.0	446
					136	25.0	448
					137	25.0	449